Bulletin 109

DEPARTMENT OF THE INTERIOR

FRANKLIN K. LANE, SECRETARY
BUREAU OF MINES
VAN. H. MANNING, DIRECTOR

OPERATING DETAILS OF GAS PRODUCERS

BY

R. H. FERNALD



WASHINGTON GOVERNMENT PRINTING OFFICE 1916 The Bureau of Mines, in carrying out one of the provisions of its organic act—to disseminate information concerning investigations made—prints a limited free edition of each of its publications.

When this edition is exhausted, copies may be obtained at cost price only through the Superintendent of Documents, Government Printing Office, Washington, D. C.

The Superintendent of Documents is not an official of the Bureau of Mines. His is an entirely separate office, and he should be addressed:

Superintendent of Documents,

Government Printing Office,

Washington, D. C.

The general law under which publications are distributed prohibits the giving of more than one copy of a publication to one person. The price of this publication is 10 cents.

First edition August, 1916

CONTENTS.

	P
Introduction	
Present status of producer-gas plants	
Producer-gas plants in Europe	
Slagging gas producer	
Producer-gas plant compared with steam turbine	
Character of fuel used in gas producers	
Tests of low-grade fuel	
Data on fuel used at commercial plants	
Pounds of fuel per square foot of fuel-bed area per hour	
Fuel consumption of up-draft plants using anthracite coal	
Fuel consumption of up-draft plants using bituminous coal	
Fuel consumption of up-draft plants using lignite	
Fuel consumption of up-draft plants using wood	
Fuel consumption of down-draft plants using bituminous coal	
Fuel consumption in down-draft gas producer using lignite	
Fuel consumption of double-zone plants using bituminous coal	
Conclusions regarding coal consumption	
Pounds of fuel per horsepower-hour	
Depth of fuel bed	
Composition of gas	
Heat value of gas	
Cubic feet of gas per pound of fuel	
Time between fuel charges and weight of fuel charges	
Time between pokings of fuel bed	
Trouble from holes and channels in fuel	
Methods of overcoming variations in quality of gas	
Methods of cleaning gas generators	
Serious cleaning troubles	
Time between periods of drawing producer fires	
Methods of scrubbing and cleaning gas	
Time between renewals of scrubber material	
Opinions regarding scrubbing and cleaning results	
Manner in which tar gives trouble	
Trouble caused by lampblack	
Relation of tar or lampblack in engine to cost of lubrication	
Burner trouble caused by tar and lampblack	
Trouble from sulphur in producer gas	
Proportion of sulphur allowable in fuel	
Auxiliary power used	
Trouble from producer auxiliaries.	
Time required to bring gas producers to full gas production after stand-by	
Stand-by fuel	
Quantity of water used by producer plants	
Quantity of vaporizer water used	
Quantity of scrubber water used	
Quantity of water required to cool engine.	

CONTENTS.

	Page.
Lubricants used	56
Preignitions and their causes	57
Changing or cleaning igniters	59
Gas pressures and distances for gas delivery	60
Recovery of by-products from waste liquors from scrubbers, washers, etc	60
Commercial use made of tar produced	60
Commercial utilization of carbon residue from oil-gas producers	61
Enrichment of producer gas	61
Temperature required at furnace	61
Spare capacity and power actually available	61
Uses of producer-gas plants.	62
Response of producer to sudden changes in demand	63
Period of continuous operation	64
Reliability and length of service of plants	66
Publications on fuel technology	69

OPERATING DETAILS OF PRODUCER-GAS INSTALLATIONS.

By R. H. FERNALD.

INTRODUCTION.

In 1900, as far as available records show, there were only two producer-gas power installations in the United States.

In June, 1915, the number probably exceeded 1,000. Of this number, some 84.5 per cent comprised small plants using anthracite, and only about 15 per cent of the total number utilized bituminous coal and lignite. In addition to these, two plants used wood, and three or four used oil.

In the main, however, the larger sized units are operating on bituminous coal and lignite.

During the early years of these plants little success was anticipated from the use of bituminous coals and lignites, but in 1904 and 1905 it was fully demonstrated at the Government testing station at St. Louis that these fuels could be utilized to excellent advantage. However, although many producer-gas plants in daily operation are using bituminous coal and lignite, many power-plant men are still skeptical regarding the successful commercial use of these fuels.

PRESENT STATUS OF PRODUCER-GAS PLANTS.

In this connection the author can offer no clearer idea of the present status of the producer-gas power plant than is presented in his letter of March 4, 1915, to the prime movers committee of the National Electric Light Association in response to general queries from the committee. The text of the letter follows:

In response to your request for a brief summary of the producer-gas situation, I take pleasure in submitting herewith a brief outline of some of the more important phases of this development and in answering the queries that you have put to me.

1. General classification of gas producers.—Producers for power purposes can be broadly classified as (a) up-draft, (b) down-draft, (c) double-zone.

In the up-draft plant the pressure in the gas generator may be greater or less than that of the atmosphere. If it is greater than that of the atmosphere, the plant is known as an up-draft pressure plant. If it is less than that of the atmosphere, the plant is commonly called an up-draft suction plant, although this reduction of pressure in the gas generator of the larger plants is now usually produced by means of an exhauster instead of by the suction stroke of the engine.

2. Producers for anthracite coal.—Little difficulty has been experienced in handling good grades of anthracite coal in gas producers. Occasionally some trouble is experienced owing to the character of the ash or to a low ash-fusing temperature. In the main, however, this fuel has been found satisfactory. For most sections of the country the price of anthracite is relatively too high to warrant its use in plants of large capacity. It is, therefore, largely utilized in plants not exceeding 500 horsepower. As far as I know little has been done in this country with gas producers for the utilization of anthracite screenings or material from the culm pile.

Anthracite coal may be utilized to good advantage in plants of either the up-draft or the down-draft type. Inasmuch as it is comparatively free from tar, anthracite is commonly used in the up-draft producer of either the suction or the pressure type. A single installation of 4,000 horsepower of down-draft producers is using anthracite at \$11.30 a ton in preference to bituminous coal for which the plant was designed. Although the company owns bituminous mines, it places a value of \$8 a ton on its books for the bituminous coal. On this basis of \$8 a ton for the bituminous coal and \$11.30 a ton for the anthracite, a year's operation shows financially in favor of the anthracite. Outside of two or three installations, the individual anthracite plants of this country do not exceed a few hundred horsepower.

3. Bituminous coal.—Satisfactory gas producers have been designed for the use of both bituminous coals and lignites of good quality. There is comparatively little difficulty in handling on a commercial scale such plants, provided the fuel is low in ash, has a fairly high ash-fusing temperature, and does not give serious trouble from caking and clinkering. Unfortunately these restrictions are too exacting to fit our common practice in the United States with low-priced fuel. The European situation, where they are able to specify rather definitely the characteristics of the coal, is very different.

My answer, therefore, to your query as to whether producers have been successfully designed for the use of bituminous coals and lignites is "yes" for bituminous coals and lignites of high grades.

I do not say "no" for other grades of bituminous coals and lignites, but I realize that low-grade fuel, high in ash and prone to clinker troubles, is not regarded in the majority of cases as worth the time and effort required. Bituminous coals and lignites of good grade may be successfully used in the up-draft producer if adequate equipment is installed for scrubbing the gas and removing the tar, in the down-draft producer of the continuous type, and in the double-zone producer.

The largest single generator in the United States with which I am familiar is one of 250 square feet of fuel-bed area, burning between 3,000 to 4,000 pounds of Illinois bituminous coal per hour. I see no reason why single-shell producers of this type should not be built four times this capacity.

4. My estimate of the horsepower capacity of gas producers installed in the United States for power purposes is as follows:

For anthracite coal:

Plants of more than 500 horsepower rating, horsepower	40,000
Plants of less than 500 horsepower rating, horsepower	
For bituminous coal, horsepower	130,000
For lignite, horsepower	15,000
My estimate of the annual fuel consumption of these plants is, roughly	:
Anthracite coal, short tons	240,000
Bituminous coal, short tons	400,000

a These figures were reported at the time of making the installations. The latest reports (June, 1915) give the fuel-bed area as 210 square feet and the average fuel consumption as 2,750 pounds per hour.

Lignite coal, short tons.....

- 5. In response to your query regarding the slow progress in the development of the bituminous-coal producer, I name the following as among the reasons that immediately suggest themselves:
- (a) The low price of our fuels. The time has seemingly not yet arrived when there is sufficient demand for reduced operating costs to warrant the investment necessary for the production of producer-gas units of sufficient size to seriously compete with the efficient steam-turbine units of the present day.
- (b) As a corollary to a, the cost of the labor involved and the reduced capacity limit producers to the utilization of fuels of good grade. As soon as the cost of fuel is sufficiently high to warrant the use of high ash, low-grade material the design of a producer for this purpose will be speedily forthcoming.
- (c) Additional difficulties are satisfactory gas cleaning, tar removal or recovery, elimination of sulphur, and the prevention of serious clinkering. All of these difficulties can, I believe, be obviated.
- (d) The fact that, up to the present time, no gas engine has been developed of sufficient size to enter into serious competition with the recent steam-turbine units of 30,000 kilowatt and 35,000 kilowatt capacity.

PRODUCER-GAS PLANTS IN EUROPE.

In considering the many phases of this problem you will, I believe, be interested to know the trend of European producer-gas practice to-day. I therefore append a few notes gleaned from my inspection last summer in the interest of the United States Bureau of Mines.

We find in Europe a demand for a gas producer to handle all grades of fuel, especially those grades usually sent to the dump. This demand has brought to the European market the revolving, eccentric-grate producer. Among the most important advantages claimed for these producers is automatic ash removal. Dependent on this primary advantage rest the following claims for the revolving grate:

- 1. Low labor cost for handling ashes.
- 2. More uniform and more complete combustion.
- 3. Operation for months without interruption.
- 4. Ability to handle much more fuel per square foot of fuel-bed area.
- 5. Less space per 1,000 cubic feet of gas produced or per horsepower of plant.
- 6. Freedom from dust and the usual excessive heat and dirt during removal of ashes.
 - 7. Production of a gas of nearly uniform quality.
 - 8. Reduction in the cost of upkeep.

If in addition to rotating the grate the grate be placed slightly off center, a feature is introduced that is probably of far greater value in handling high-ash, clinkering fuels than the mere rotation of the grate.

Experience with European fuels has shown that even with the eccentric revolving grate and the usual producer shell construction clinker troubles are not entirely eliminated when poor-grade fuel with low ash-fusing temperature is used. A further important feature—probably the most important single item—for overcoming clinkering and the tendency of the ash to fuse with the producer lining is the water jacketing of the part of the producer shell surrounding the hot zone.

These revolving grate producers are reported to gasify two to three times as much fuel per square foot of fuel-bed area per hour as can be gasified in corresponding updraft producers with fixed grates.

Claims of very low percentages of carbon in the ash are also made for this type of producer, the reported record for one installation being 5 per cent carbon, or 0.47 per cent of the fuel gasified.

The claims advanced regarding the steam requirements for clinkering coals used in producers with water jackets around the hot zone are to the effect that not over one-quarter as much steam is required as in the jacketless type with fixed grate. The figures given for comparison are 1 pound of steam per pound of fuel for the fixed-grate jacketless producer and 0.29 pound for the revolving eccentric-grate producer. Results with United States coals in fixed-grate jacketless producers indicate that 1 pound of steam per pound of coal is rather high for plants of good size. Seven-tenths of a pound is nearer the figure, although there are undoubtedly many plants, indifferently operated, that are not below the 1-pound rate.

Representatives of companies handling eccentric revolving-grate producers say that they handle coal containing 45 to 55 per cent ash with perfect ease and are satisfied that these producers can meet the conditions required for American high-ash caking coals.

In Europe we also find a great deal of attention given to the by-product gas plant. These plants are not of a few horsepower capacity, but the installations range from 5,000 to 30,000 horsepower. One company alone reports the installation of by-product recovery producer-gas plants using a total of 3,000 tons of fuel per day and aggregating approximately 300,000 horsepower. The capacity and purpose of a few of the larger installations are as follows:

Installa- tion No.	Fuel capacity per day.	Purpose of plant.	Installa- tion No.	Fuel capacity per day.	Purpose of plant.
1	Tons. 320	Recovery of by-products from waste fuels. Gas used for firing boilers and for power.	5	Tons. 135	Power, forge, and plate fur- naces, fire-clay kilns, etc. Power and firing caustic pots.
2 3	270 250	Central distributing station. Power and chemical pur-	7 8	120 120	Evaporating brine Power and chemical furnaces.
3	230	poses, calcining ore, etc.	9	100	Firing chrome furnaces.
4	150	Special plant for the recovery of by-products. Gas used for firing colliery boilers.	10	100	Chemical furnaces.

Capacity and purpose of a few of the larger European producer-gas plants.

The majority of these plants are used for power development and gas heating; the recovery of by-products, such as sulphate of ammonia, tar, etc., are secondary factors in the operation of the plant. On the other hand, there are several installations in which power is the secondary factor, the plant being run primarily for the valuable by-product, sulphate of ammonia, which brings a commercial return of \$50 to \$60 a ton.

A few plants are operated for the by-products alone. In certain districts in which the manufacturing and industrial interests do not offer a market for the gas the so-called "by-products" become the main products and the true by-product, producer gas, is thrown away. This condition of affairs is peculiarly true in regions in which the fuel runs high in nitrogen. It is reported that an extensive plant of this character is soon to be erected in Africa.

Peat seems to be peculiarly adapted to the requirements for the production of sulphate of ammonia, and several commercial by-product plants using this fuel are now in operation in Europe. Among these are two plants in Italy using, respectively, 140 and 90 tons of peat per day.

One of the most interesting plants visited last summer was a by-product coke plant, in which the coke-oven gas was the main product and the coke the by-product, combined with a by-product producer-gas plant. The coke-oven gas was turned into the city mains for general use. In order to obtain all this gas for sale to the city, a distinct

central producer-gas plant was installed, as the poorer grade gas, which was not available for general city use, was entirely satisfactory for heating the coke ovens. The originator of this combined method says: "The great advantage of this system is the fact that coke breeze and low-grade fuel generally can be used in the producers without lowering the efficiency of the plant." The producer plant consists of five units, each of 20 tons capacity a day. The coke from the ovens, which is regarded as a byproduct, finds a ready market for blast-furnace work, and it is estimated that the byproducts from the producer plant, sulphate of ammonia and pitch, practically pay the cost of operation of the producer-gas installation. The coal used in the producers is double-screened nut and contains no dust. It is a fine-looking coal and is reported to be high in oils.

The several companies manufacturing by-product gas plants believe that there is a large field for such plants in the United States if the fuels used be carefully selected. They regard our caking coals as bad for this type of plant.

SLAGGING GAS PRODUCER.

The blast-furnace type or slagging gas producer has appeared at regular intervals in Europe and investigations along this line have also been conducted in this country both by commercial interests and the United States Bureau of Mines. In spite of the many claims that no such producer can operate with any commercial success, we find at a colliery in Deutsch-Luxemburg a wonderfully interesting installation consisting of four slagging producers. These producers are approximately 10 feet in internal diameter and gasify 60 tons of fuel each per 24-hour day. The first of these producers was installed about two years ago and required much study and many changes. At the present time [March 4, 1915] these producers are working on 10 per cent ash fuel, but the company anticipates utilizing material containing 20 to 30 per cent ash. Several different companies are reported to be using these slagging producers, and the fact that this type of producer has a real commercial position is shown by the catalogue of one of the large producer manufacturers of Germany, which, among several other classifications, lists its producers as—

- (1) Producers with rotating grates.
- (2) Slagging producers.
- (3) Flat-grate producers.
- (4) Step-grate producers.

Considerable interest is also manifested abroad in the use of wood refuse and similar material in gas producers. At the present time, however, these plants are of small size.

The interest of engineers in Europe is also more or less centered on the possibilities of powdered fuel and questions relating to low-temperature distillation. The principal purpose of this latter problem is to procure a clean smokeless fuel for the unlimited number of fireplaces and at the same time to recover from the original fuel large percentages of oils, motor spirits, and ammonia.

In conclusion, I believe that the time is not distant when the price of our coals must necessarily materially increase. When this time does come we will look much more seriously on the important problems connected with our fuel conservation. We will find it imperative to use high-ash low-grade fuels which, in many cases, will have a low ash fusing temperature. Transportation of this high ash material will be out of the question and its conversion into gas at the mines will result. Even though large gas engines are not forthcoming, the economic use of grades of material that can not be utilized directly under steam boilers will warrant large installations for the production of producer gas and its use for steam generation for large turbogenerator units with long-distance electric transmission.

PRODUCER-GAS PLANT COMPARED WITH STEAM TURBINE.

The steam turbine naturally lent itself to central-station service. It was a unit easily understood by steam-engine operators in so far as practical operation is concerned; it could be readily erected without radical changes in the boiler-room equipment; and it rapidly met the demand for large central-station units.

The producer-gas plant was an untried factor; it met with strong opposition from the older steam-plant operators, who saw possibilities of being forced out of their positions; its installation meant a complete renovation of the entire plant, with the replacing of the steam boiler by the producer unit. Large units of this type did not materialize, with the natural result that even to-day the producergas power plant is not the large central-station unit, although it occupies a strong position among the isolated plants and the small central stations.

Methods of operation vary greatly with local conditions and especially with the personal inclination or opinion of the plant superintendent. This variation is, perhaps, perfectly natural, owing to the newness of producer-gas power, the absence of experienced producer-gas engineers, the absence of cooperation among the operators of these independent isolated plants, and the absence of well-defined commercial investigations.

With this lack of a common interest on the part of the owners or operators of these plants—an interest that has of late tended to place central-station operation on somewhat uniform basis—no standards for comparison of plant operations have appeared and little has been known by the superintendent of one plant regarding the relative efficiency of operation of his own installation and that of another plant of similar type operating under similar conditions.

Several unsuccessful attempts have been made by various organizations to collect data relating to these important matters, but unfortunately little or no information could be had.

Appreciating the value of such data in connection with the many problems of fuel conservation and its investigations into the use of producer-gas power, the Bureau of Mines decided (1) that an effort should be made to procure operating details from a small number of representative producer-gas plants using scrubbed gas either for power or heating purposes; (2) that primarily data from plants using bituminous coals and lignites should be sought, but that data from a few of the larger anthracite plants and the oil and wood plants should be included.

With these points in mind, data sheets were sent to the owners of a limited number of plants, and for the most part the response has been highly gratifying. Returns of a positive character were received from 39 installations.

Although, as might be expected, a great deal of indefiniteness exists regarding many of the operating details, and few, if any, cost data are available, it is believed that in the following pages sufficient detailed information is presented to provoke wholesome discussion on the part of those interested in this form of power; to stimulate responses to future requests from the Bureau of Mines, and to serve as a basis for comparison by the different operators of similar plants.

CHARACTER OF FUEL USED IN GAS PRODUCERS.

Owing to the agitation of the Bureau of Mines for several years past concerning the use of high-ash and low-grade fuels, it was hoped that several producer-gas installations would report the use of grades of fuel hitherto regarded as of little commercial value. However, an inspection of several plants in 1913 showed rather conclusively that on the whole the grade of fuel used in producer-gas installations has been steadily rising, and, in the main, the fuel used to-day is decidedly superior to that used six or eight years ago.

Although from the standpoint of the engineers of the Bureau of Mines this condition is to be regretted, it is perhaps perfectly natural, as the tendency of the operators of such plants is to reduce manual labor to a minimum. A feeling of assurance by the management of guaranteed reliability of service is also commercially important in determining the quality of fuel to be used. It is not strange, then, that the highest grade fuel obtainable at a reasonable price is, in nearly every instance, the one adopted.

A rather poor grade of bituminous coal was originally used in a plant of considerable size, but owing to the amount of labor required in operating, the purchasing agent was finally persuaded by the plant superintendent to substitute a high-grade coal at a much higher price per ton.

Such excellent results were at once obtained and the labor cost was so materially reduced that the purchasing agent, who had formerly believed in purchasing the cheapest coal to be had, immediately substituted the high-grade coal throughout the boiler plant as well as the producer plant. The superintendent felt that the greatest service the producer plant had rendered was in improving the grade of fuel used in the steam plant. He stated that he realized that his company was not working toward fuel conservation, but he felt that reliability of service was the uppermost requirement in his plant. He said that he would be glad to use a lower grade fuel at a less cost per ton if he could be shown plants with similar exacting commercial requirements successfully operating on such fuel.

Such comments are, for the most part, typical of the present situation. It is, however, gratifying to note here and there excep-

tions to this tendency. One notable example may be seen in Texas in a plant that uses lignite screenings as the regular fuel for the gas producers. The manager finds these screenings, costing much less than run-of-mine lignite, an excellent producer fuel. He has given a standing order for this material, but has considerable difficulty in procuring enough of it.

As far as is reported, no other operator in that vicinity feels any assurance of success with such screenings as they are generally regarded as inferior fuel.

The high character of the fuels generally used for producer-gas installations is made apparent by the data in the table following.

Grade of fuel used in different types of gas producers.

PRODUCERS USING BITUMINOUS COAL.

Plant No.	Ash.	Sulphur.	Heating value per pound as fired.
24	Per cent. 3.7 6.9 7.4 10.1 6.7 7.0 5.0 7.9 4.8 7.3 5.5 7.0	Per cent. 0.5 1.6 .5 3.4 2.2 1.5 .9 1.2 .5 .8 1.0 2.0	B. t. u. 11, 540 12, 270 12, 296 12, 522 13, 741 13, 750 14, 000 14, 370 14, 535 14, 769 14, 800 14, 834
PRODUCERS USING LIGNITE.	7.9	1.0	5, 560
PRODUCER USING WOOD.	6. 9 8. 2 6. 0	.6 .4	7,440 7,070 11,400
26			5,400

Most lignite contains 30 to 40 per cent water, but, as indicated above, it does not necessarily run high in ash. As regards true fuel conservation, there is seemingly little being done in the United States by the operators of producer-gas plants.

TESTS OF LOW-GRADE FUEL.

It is, perhaps, important again to emphasize the possibilities from high-ash coals. Although it is fully appreciated that commercial conditions make reliability of operation and plant capacity imperative, it is the belief of the author that many of these plants could utilize relatively cheap, poor grades of fuel with an assurance of both reliability and capacity and a net financial gain. The most difficult problem seems to be that of procuring thoroughly competent men for the careful supervision of such installations. The tabulated figures following, showing the results of Bureau of Mines tests, indicate the possibilities of using in gas producers the fuels represented.

Results of fuel tests, showing adaptability of certain fuels for use in gas produ	Results	of fuel tests.	showing ac	laptability of	f certain fuel	s for use in	gas producer
---	---------	----------------	------------	----------------	----------------	--------------	--------------

Source of fuel.	Variety or size of fuel.	Ash.	Moisture.	Quantity of fuel, as fired, con- sumed in producer per brake horsepower- hour.
New Mexico. Tennessee. Iowa. Wyoming. Do. Illinois. Brazil, South America. West Virginia. Pennsylvania Do. West Virginia.	Run of mine	Per cent. 19. 63 20. 57 20. 70 20. 72 21. 73 23. 12 23. 44 28. 08 30. 35 31. 89 43. 74	Per cent. 3.62 3.55 16.69 9.44 8.65 8.67 10.96 2.91 2.68 2.25 .47	Pounds. 1. 10 1. 45 1. 56 1. 70 1. 83 2. 88 2. 02 1. 26 2. 34 2. 76 1. 65

If these figures are compared with the results on page 25, it will readily be seen that even after due allowance has been made for the difference between the operation of a testing station and that of the average commercial plant, the possibilities from these high-ash fuels warrant thoughtful consideration by the progressive managers of commercial installations.

The manager of a large steel plant in England realizes that his ability to maintain the high-grade qualities of the steel, for which his company has been so long noted, and at the same time to reduce the cost of manufacture to a point below that of his competitors depends on a reduction in the cost of generating power. He is, therefore, seriously attacking the immense refuse heaps that have been accumulating for years at the colliery connected with the steel plant. The material from these refuse heaps is passed through a crusher and then to a washer where approximately one-half of the nonconbustible material is removed. The washed fuel, containing approximately 25 per cent of noncombustible material is then utilized in rotary eccentric-grate producers, to the entire satisfaction of the company and with a reduction in the cost of the product of the plant.

In sharp contrast is a plant of several thousand horsepower previously mentioned. This plant is operated in the interests of a large corporation in the United States, which owns extensive bituminous-

coal mines not distant from the plant. The operating company sends its own bituminous coal to the market and uses Pennsylvania anthracite at a cost of over \$11 per ton in its producer-gas plant. Owing to the lower labor charge when anthracite is used, the records of the plant show, for periods of a year or more, that the cost of operation with bituminous coal, if charged on the books at \$8 per ton, is considerably more than with anthracite coal. Although at the prices indicated, the anthracite fuel seems to give the better results, it is a question of no little importance as to whether refuse material from the company's mines might not, even with higher labor costs, prove the least expensive fuel, especially as the plant has ample spare producer capacity.

DATA ON FUEL USED AT COMMERCIAL PLANTS.

The Bureau of Mines sent form letters to numerous producer-gas plants, inquiring as to the character of fuel used, the reasons, if any, for having changed fuels, the reasons why certain plants did not use local fuels, and the necessity for a low sulphur content in the coal. The responses may be briefly summarized as follows, the numbers being those assigned to the replies as received. The figures for fixed carbon, volatile matter, moisture, sulphur, and ash are percentages:

Summary of replies to queries regarding operation of producer-gas plants.

UP-DRAFT PLANTS.

Plants using anthracite.

- 1. Fuel, buckwheat. Low-sulphur coal necessary, as high-sulphur coal causes back-firing.
- 9. Fuel, buckwheat. Pea coal has been used. Buckwheat is fully as cheap and works nearly as well. Low-sulphur coal not necessary for successful operation.
 - 16. Fuel, buckwheat, from \(\frac{3}{8}\)-inch down. Analysis follows:

Fixed carbon	82.47
Volatile matter	5.29
Moisture	
Ash	12.29

This plant formerly used gas-house coke, but the anthracite works with greater ease, as the coke clinkered badly and gave trouble from tar in the engines.

- 19. Fuel, Pennsylvania No. 1 buckwheat. Low-sulphur coal regarded as necessary to prevent clinkering.
- 20. One 200-horsepower producer uses pea anthracite, and one 250-horsepower producer uses run-of-mine bituminous coal. The pea anthracite is used in the spare producer, the other producer having been modified for the use of coke, which is a by-product from the gas department.
- 36. Fuel, No. 1 buckwheat. Pea anthracite formerly used. Buckwheat costs less and seems to give about the same results.

Plants using bituminous coal.

3. Fuel, Pocohontas slack. Analysis follows:

Fixed carbon	73. 6 0
Volatile matter	17.70
Moisture	1.45
Ash	7.25
Sulphur (separately determined)	. 80
British thermal units in coal, as fired	14,800

Formerly used Alabama coal. Unsatisfactory. Too much tar. Caused preignition and variable gas quality. Peat is mined in the vicinity. Was tried, mixed with coal, and did fairly well, but gave an offensive, sickening gas. No ill effects from sulphur in coal, except possibly in causing coal-pile fires.

- 5. Fuel, bituminous coal from Puritan mines, Cambridge, Ohio, 3-inch lump. Have experimented with other coals, but the above meets requirements best. Other coal is mined in the vicinity, but it is too high in sulphur. Low-sulphur coal is required, as the sulphur fumes cause distress.
- 12. Fuel, No. 2 washed nut bituminous coal that passes over a 3-inch and through a 24-inch screen. The proximate analysis is:

Fixed carbon	54 . 83
Volatile matter	29.91
Moisture	7. 90
Ash	7.36
Sulphur (separately determined)	. 48
British thermal units in coal as fired	12,296

Low-sulphur coal is regarded as essential in the operation of this plant to prevent sulphur fumes throughout the factory and a sulphur coating on the manufactured product as the gas is used for annealing.

17. Fuel, Hocking Valley coal in nut sizes passing over 1-inch and through 2-inch screens. The two grades used show—

Fixed carbon	51.67	57. 60
Volatile matter	38. 26	34. 20
Moisture	9. 24	4.99
Ash	10.07	3. 21
Sulphur (separately determined)	3.42	. 73
British thermal units in coal as fired		13,658

The second fuel is reported to give not enough gas and to be too high in by-products. 21. Owing to the fact that the gas is used in connection with furnaces and the products of combustion are discharged into the room, considerable irritation of the lungs and throat is experienced, which seems to cause ill health among the employees unless the percentage of sulphur in the fuel is kept low. The fuel used contains less than 1 per cent sulphur.

25. Fuel, Hocking Valley bituminous nut coal. The analysis follows:

Fixed carbon	47. 01
Volatile matter	36. 67
Moisture	9. 30
Ash	6. 97
Sulphur (separately determined)	1.98

The company used anthracite for the first two years, but on the addition of new producers changed to bituminous coal, with a saving due to the difference in price. They find that the present plant operates more easily on bituminous coal than the former producers did on anthracite.

33. The analysis of the fuel used follows:

Fixed carbon	69. 2
Volatile matter	21.3
Moisture	2. 5
Ash	7.0
Sulphur (separately determined)	1.5
British thermal units in coal on dry basis	14,760

- 37. Fuel, bituminous, Westmoreland (Pa.) run-of-mine coal, showing 14,200 British thermal units on the dry basis. Anthracite coal is mined within 50 miles, but the bituminous coal works more freely and is less expensive.
- 39. Fuel, New River and Pocahontas (W. Va.) coal reduced to extreme fineness before received. Typical analysis of the New River coal follows:

Fixed carbon	73. 6
Volatile matter	20.4
Moisture	1.04
Ash	4.96
Sulphur (separately determined)	. 91
British thermal units in coal as fired (approximately)	14,500

Considerable carbon in ash at times because of uneven burning of fuel bed. Have used Pocahontas. No difference noted in general operation between Pocahontas and New River. Some wood is available in the vicinity, but the high cost of procuring it and the uncertainty as to successful gasification in the producers installed prevent its use. No effects, ill or otherwise, have been noted from sulphur.

Plants using lignite.

4. Fuel, Texas, screened, large-lump lignite. Analysis of coal as received:

Fixed carbon	27.02
Volatile matter	36. 92
Moisture	29. 20
Ash	6.86
Sulphur (separately determined)	. 58
British thermal units in coal as received.	

Obtain better gas with coal of low-sulphur content.

11. Fuel, lignite screenings from two mines, showing a proximate analysis as follows:

	Mine 1.	Mine 2.
Fixed carbon	17.50	12.13
Volatile matter	47.55	48. 18
Moisture	27.21	31.81
Ash	8. 21	7.88
Sulphur (separately determined)	. 44	1.03
British thermal units in coal as fired	7,073	5,561
British thermal units in coal on dry basis	9,717	8,153
British thermal units in coal combustible	10,952	9,217

Formerly this plant used lignite lump, but the cheaper grade gives satisfactory results. This cheaper fuel is regarded by the mine operators as of lower grade than the lignite lump. It is lower in heat value and is also of a grade not usually marketable. It works with slightly less ease than the lump lignite, but as it costs less and is really worked with little difficulty it is regarded as a very satisfactory fuel. This lignite is mined in the vicinity of the plant. Low-sulphur fuel is not regarded as essential for successful operation.

38. Fuel, lignite, pea-screenings, near Centralia, Wash. Several other Washington lignites have been tried, but all cost more and were no better or not so good on account of hotter fire and more clinker. The present fuel is of lower grade and highest in ash but works better.

Plants using wood.

- 13. Fuel, waste hardwood in lengths of 1 foot or less, and about 1 to 3 inches in diameter, together with some bark and sawdust. This hardwood runs about 35 to 60 per cent moisture as used. During the early operation of the plant sticks 1½ to 3 feet long were used, but some difficulty was experienced with arching of the fuel bed and the formation of pockets that burned out the gas.
- 26. Fuel, cypress refuse from the hog machine. Brought about 1 mile from the mill. Chips and sawdust also used. The wood as fired yielded 5,400 British thermal units, and on dry basis 10,000 British thermal units. Other fuels tried in this plant are: Anthracite, bituminous coal, coke breeze, and pine hog. Coal or coke was found inferior to the wood refuse, as the cypress hog gives a more constant quality of good gas. It works with greater ease and costs less than the other fuels. Low sulphur content is regarded as important because of the deleterious action of $\rm H_2SO_4$ on the producer plant and engine.

DOWN-DRAFT PLANTS.

Plants using bituminous coal.

8. Fuel, Big Muddy (Ill.) run-of-mine coal. Analysis follows:	
Fixed carbon	50.92
Volatile matter	32.80
Moisture	9.40
Ash	6.88
Sulphur (separately determined)	
British thermal units in dry coal	13, 553

Satisfactory in price and results. Is regarded as high grade. Makes good gas with little clinker. No trouble has been experienced on account of sulphur.

20. One 200-horsepower producer uses pea anthracite and one 250-horsepower producer uses run-of-mine bituminous coal with—

Fixed carbon	76.80
Volatile matter	17.11
Moisture	. 1.39
Ash	4.70
Sulphur (separately determined).	1.01

The pea anthracite is used in the spare producer, the other producer having been modified for the use of coke, which is a by-product from the gas department.

22. Uses Pocahontas slack. Analysis follows:

Fixed carbon	81.41
Volatile matter	13.23
Moisture	. 54
Ash	4.82
Sulphur (separately determined)	. 50
British thermal units in slack as fired	14, 769

Experiments have been made with other fuels, but no other fuel has been used for any length of time. The lower the sulphur the better the results.

23. Fuel, West Virginia bituminous coal run through a 4-inch crusher.

Fixed carbon	53.89
Volatile matter	36.01
Moisture	3.45
Ash	6.65
Sulphur (separately determined)	2.22
British thermal units in coal as fired (average of 49 cars)	13,741

This company has used other West Virginia coals and Indiana coal but finds the present coal gives a larger producer output. It is of higher grade than the other fuels tried, higher in carbon, lower in ash, and works with greater ease. It costs more than the other fuels.

24. Fuel, bituminous southwestern Illinois coal, 1½ to 7 inches. Analysis follows:

Fixed carbon	55.51
Volatile matter	31.78
Moisture	9.02
Ash	3.69
Sulphur (separately determined)	
British thermal units in dry coal	12,805

Run-of-mine coal from the same mine and a few other similar Illinois coals have been used. The run-of-mine coal was changed because of too much slack, as a more uniform grade of coal is preferred. The present fuel is regarded as of higher grade than that previously used, although it comes from the same mine. It is freer from dirt and of more suitable size for producer use. It operates with greater ease. It costs more per ton at the mine. Low sulphur is not essential but is preferred.

27. Fuel, Pennsylvania run-of-mine bituminous coal. The average analysis of the coal in four cars follows:

Fixed carbon	76.94
Volatile matter	
Moisture	1.47
Ash	7.89
Sulphur (separately determined)	1.18
British thermal units in coal as fired	14,535

When this particular grade of coal can not be procured a coal yielding 13,365 British thermal units is substituted. The latter fuel is higher in volatile matter, ash, and sulphur, and lower in fixed carbon. It is not necessary to run the fires quite as hot as with the former fuel on account of the higher volatile matter. The second coal costs less than the first. Low sulphur content is regarded as essential. On account of corrosion the 3-inch steel economizer tubes last only about 18 months.

- 28. Fuel, West Virginia Pocahontas coal, running from dust to 0.75 inch in size. As fired it yields 13,500 to 14,000 British thermal units, and on the dry basis it yields 14,000 to 14,500 British thermal units.
- 29. Fuel, Virginia bituminous run-of-mine coal and slack. Washed slack has been used, but a change was made to the fuel first mentioned because no more washed slack could be purchased. The present fuel is regarded as of lower grade, although it works better in the producer and costs less.
 - 35. Fuel, Berwyn and White Scalp level, South Fork (Pa.) coal. Analysis:

Fixed carbon	77.0
Volatile matter	17.0
Moisture	. 5
Ash	5.5
Sulphur (separately determined)	1.0
British thermal units in coal as fired	

This is a higher-grade coal and costs more than that previously used. The change was made as better results can be obtained with the present coal, as it works with greater ease and does not cake or clinker. Low sulphur content is regarded as necessary in order to eliminate the action of sulphuric acid.

DOUBLE-ZONE PLANTS.

Plants using bituminous coal.

- 2. Fuel, New Mexico bituminous chestnut coal. Costs less than coal previously used in steam plants. Low-sulphur coal not necessary.
 - 8. Fuel, Big Muddy (Ill.) run-of-mine coal. Analysis follows:

Fixed carbon	50.92
Volatile matter	32.80
Moisture	9.40
Ash	6.88
Sulphur (separately determined)	1.56
British thermal units in coal on dry basis	13,553

Satisfactory in price and economy. It is regarded as high grade. Makes good gas with little clinker. No trouble has been experienced on account of sulphur.

Plants using lignite.

31. Fuel, lignite, size about 3-inch cubes.

Fixed carbon, approximately	40
Volatile matter	34
Moisture	18
Ash	6
British thermal units in coal as fired	11,400

POUNDS OF FUEL PER SQUARE FOOT OF FUEL-BED AREA PER HOUR.

One of the most important commercial items connected with the design and the operation of gas producers is the determination of the number of pounds of fuel consumed per square foot of fuel-bed area per hour. This rate of fuel consumption varies radically with different types of plants and with different grades and different types of fuel and has led to much difficulty in designing and in rating producers. Early work in this country followed European practice almost entirely and thereby occasioned much trouble in connection with the rating of pioneer plants, and brought about the ultimate failure of many of them. Under certain European conditions fuels of a definite grade are specified, so that high rates of fuel consumption may be obtained. It is not impossible to obtain similar rates of consumption under corresponding circumstances in this country, but as selected fuels are seldom obtainable except for special tests, it has been found that in general in the United States the rate of fuel consumption per square foot of fuel-bed area does not average much over one-half the consumption originally guaranteed by early manufacturers. This fact has, of course, led to a decided modification in the design of many plants.

Although the possible rate of burning high-grade fuel may be relatively high, much depends on the method of operation and the character of the fuel as to the actual commercial results obtained. Certain types of fuel lend themselves more readily to high rates of fuel consumption than others, and with a given fuel the rate of burning will vary with the nature of the gas-generating process, the downdraft plant consuming practically twice as much fuel per square foot of fuel-bed area per hour as the up-draft. In 1911 the writer stated that down-draft plants were in operation that consumed more than 40 pounds of lignite per square foot of fuel-bed area per hour, and that up-draft producers could gasify comparatively large quantities of fuel per hour for relatively short periods, but that in actual operation with ordinary grades of fuel it was doubtful whether the consumption in the up-draft plants would exceed 15 to 16 pounds per square foot of fuel-bed area per hour. The normal figure at that time was stated to be much nearer 10 pounds, and it was said that 10 pounds would prove to be a high figure for fuels having a large percentage of ash or a sulphur content that tended to produce serious clinkering. interesting to compare the figures mentioned with the figures from several plants in commercial operation at the present time, as furnished by the owners or operators of the plants. Such figures are presented in the pages following.

FUEL CONSUMPTION OF UP-DRAFT PLANTS USING ANTHRACITE COAL.

The fuel-consumption figures for certain plants using anthracite coal follow:

Fuel	consumntion	αf	un-draft	ane	moducers	usina	anthracite coal.	
T. WCO	CONSTRUCTOR	o_{I}	$u p$ - $u_1 u_1 v$	yus	producers	would	animache cout.	

Plant No.	Horsepower of each gas gen- erator.	Area of fuel bed.	Fuel as fired per square foot of fuel-bed area per hour.		
		ruer bea.	As rated.	As actually operated.	
14	300 300 300 400	Square feet. 7.1 12.6 38.5 42.5 44.2 44.2 56.6	Pounds. 18.0 16.0 7.8 8.7 6.8 8.5 9.0	Pounds. 12.7 7.3 4.5	

a Fernald, R. H., and Smith, C. D., Résumé of producer-gas investigations: Bull. 13, Bureau of Mines, 1911, p. 45.

The average consumption of the seven plants listed, on the basis of the manufacturers' rating, was 10.7 pounds per square foot of fuel-bed area. The number of plants reporting operating figures for anthracite coal is not enough to permit the presentation of averages, although it is probable that the average figure for commercial operation for up-draft plants using anthracite as a fuel is not far from the average given on the basis of the manufacturers' rating.

FUEL CONSUMPTION OF UP-DRAFT PLANTS USING BITUMINOUS COAL.

Figures covering fuel consumption of gas producers using bituminous coal follow:

Plant No.	Horsepower of each	Area of	Fuel as fired per squar foot of fuel-bed are per hour.		
	gas gen- erator.	fuel bed.	As rated.	As actually operated.	
		Square feet.	Pounds.	Pounds.	
37	. 200	23.7	7.0	7.0	
3		25.0	10.0	7.6	
33	. 250	28.3	10.6	7.6	
17		33.1	10.0	13.7	
12	f 200	24.0	10.4	} 7.4	
***************************************	: \frac{1}{200}	42.0	9.5	Į	
25	300	40.0	9.1 8.0	8.5	
39	100	50.0 50.2	10.0	6.1	
	650	50.0	10.0		
21	1,000	78.0	}	8.7	
5		70.9	7.0	7.1	
12		210.0	14.3	13. 1	
Average			10. 4	8.7	

Fuel consumption of up-draft gas producers using bituminous coal.

For the up-draft plants operating on bituminous coal the range of actual operating rates of fuel consumption seems to be from approximately 6 to more than 13.5 pounds per square foot of fuel-bed area per hour. This marked difference might, on first thought, be supposed to be due to differences in the character of the fuels, but an examination of the records submitted shows that actually the higher-grade fuel is used in the plant reporting the low rate of fuel consumption per square foot of fuel-bed area per hour.

The coal used in the plant reporting the 6-pound rate averaged 14,500 British thermal units as fired and contained 5 per cent ash and 0.9 per cent sulphur, whereas the coal used in the plant reporting the 13.7-pound rate averaged 12,520 British thermal units and contained 10.1 per cent ash and 3.4 per cent sulphur, and the coal in the plant reporting the 13.1-pound rate averaged 12,300 British thermal units and contained 7.4 per cent ash and 0.5 per cent sulphur.

The inference is that the plant with the 6-pound rate was operated much below the capacity of the producer.

Although there seems to be little direct relation between the rated fuel consumption for the individual plants and the number of pounds of fuel actually burned per square foot of fuel-bed area, the average figures check within reasonable limits and indicate that approximately 8.5 pounds per square foot of fuel-bed area per hour with good-grade bituminous coal is a reasonable figure for an up-draft producer gas plant.

FUEL CONSUMPTION OF UP-DRAFT PLANTS USING LIGNITE.

The figures for fuel consumption in gas producers using lignite follow:

Fuel consumption of	up-draft gas	producers	using light	iite.
---------------------	--------------	-----------	-------------	-------

Plant No.	Horsepower of each	Area of	Fuel as fired per square foot of fuel-bed area per hour.		
	gas gen- erator.	fuel bed.	As rated.	As actually operated.	
4	100 100 250 300	Square feet. 19.6 20.4 38.5 41.3	Pounds. 11.5	Pounds. 11. 5 8. 6 14. 8 8. 5	
Average			10.8	10.8	

The returns cited for lignite in up-draft plants indicate that approximately 11 pounds of lignite is burned per square foot of fuel-bed area per hour in plants of this type.

Tests at the Government testing station at St. Louis in 1904–1906 indicated that a higher average rate may easily be obtained with lignite in up-draft plants.

FUEL CONSUMPTION OF UP-DRAFT PLANTS USING WOOD.

Figures for fuel consumption in gas producers using wood follow:

Fuel consumption of up-draft gas producers using wood.

Plant No.	Horsepower of each	Area of	Fuel as fired per square foot of fuel-bed area per hour.		
	gas gen- erator.	fuel bed.	As rated.	As actually operated.	
13	150	Square feet. 50. 3	Pounds. 12.0	Pounds.	
26	$\begin{cases} 200 \\ 280 \end{cases}$	33.3 50.3	} 14.0	14.5	

FUEL CONSUMPTION OF DOWN-DRAFT PLANTS USING BITUMINOUS COAL.

Figures showing fuel consumption in certain plants using bituminous coal follow:

Fuel consumption of down-draft gas producers using bituminous co	on of down-draft gas producers using bituminous co	coal.
--	--	-------

Plant No.	Horsepower of each	Area of	Fuel as fired per square foot of fuel-bed area per hour.		
	gas gen- erator.	fuel bed.	As rated.	As actually operated.	
22. 27. 35. 28. 28. 8. 23. 24. Average.	500 800 1,500 1,500	Square feet. 17. 4 17. 4 20. 4 38. 5 50. 0 36. 0 60. 0	Pounds. 14.4 17.0 14.7 13.0 12.5 33.4 27.5 20.0	Pounds. 14.4 14.7 18.4 23.5 16.7 17.5	

For the down-draft plants of the double-generator type the figures reported are perhaps not sufficient to warrant conclusive deductions, but when compared with data from other sources they make apparent that the average fuel consumption per square foot of fuel-bed area per hour is nearly correct.

FUEL CONSUMPTION IN DOWN-DRAFT GAS PRODUCER USING LIGNITE.

Figures procured a few years since from a plant using lignite in 1,100-horsepower units of the down-draft double-generator type indicated a normal fuel rate of 33 pounds per square foot of fuel area per hour for 16 hours a day, and the unusual rate of 48 pounds for 8 hours a day. This instance, however, is too exceptional to be regarded as representative of general practice.

FUEL CONSUMPTION OF DOUBLE-ZONE PLANTS USING BITUMINOUS COAL.

Figures showing fuel consumption of double-zone gas producers using bituminous coal follow:

Fuel consumption of double-zone gas producers using bituminous coal.

Plant No.	Horsepower of each	Area of fuel bed.	Fuel as fired per square foot of fuel-bed area per hour.		
	gas gen- erator.	ruer bed.	As rated.	As actually operated.	
2	250 500	Square feet. 29.3 47.0	Pounds. 24.0 17.0	Pounds. 10.3	

As operating returns were received for only one double-zone plant, no definite direct deductions can be made, but a review of the results of tests of such a plant indicates the rate of fuel consumption under test conditions to be not far from 15 pounds per square foot of fuelbed area per hour with bituminous coal and 23 pounds with lignite.

CONCLUSIONS REGARDING COAL CONSUMPTION.

A study of the operating reports submitted indicates that the average rate of fuel consumption in producer-gas plants is considerably higher than a few years ago. This betterment is due, perhaps, to two reasons—first, a more efficient operation of the plants themselves, and, second, an increasing tendency to use higher grade fuel. The first result is to be commended, but the second should be deplored.

Although too much stress must not be laid on the following values, the deductions from the operating figures supplied above, coupled with personal observation of many other plants, seem to indicate the following approximate values for fuel consumption per square foot of fuel-bed area per hour as representative of good general commercial practice.

Figures for fuel consumption in gas producers representing good general practice.

	F	uel consun	nption per	square foo	t of fuel-be	d area per	hour with	_
Kind of plant.	Anthracite coal.		Bituminous coal.		Lignite.		Peat.	Wood.
	Average.	Maxi- mum.	Average.	Maxi- mum.	Average.	Maxi- mum.	Average.	Average.
Up-draft using— Fuel as fired. Fuel dry Down-draft using— Fuel as fired. Fuel dry. Double-zone using— Fuel dry. Fuel dry.	10.0		Pounds. 8.5 8.0 17.5 16.5 13.5 12.5	Pounds. 14.0 13.0 23.5 22.0 18.5 17.5	Pounds. 12.0 8.5 26.5 18.5 21.5 15.0	Pounds. 17. 0 12. 0 31. 5 22. 0 27. 0 19. 0		Pounds. 14.0

POUNDS OF FUEL PER HORSEPOWER-HOUR.

Producer-gas investigations of the United States Geological Survey and of the Bureau of Mines, conducted with plants not above the average in efficiency, showed the following approximate fuel consumption per brake horsepower per hour:

Results of producer-gas investigations, showing fuel consumption per brake horsepower per hour with different fuels.

	Fuel consumption per brake horsepower-hour with—							
Condition of fuel.	Bituminous coal.				Peat.a			
	Average.	Maxi- mum.	Mini- mum.	Average.	Maxi- mum.	Mini- mum.	Average.	
FiredDry	Pounds. 1.3 1.2	Pounds. 2.0 1.8	Pounds. 0.8 .8	Pounds. 2. 0 1. 63	Pounds. 2. 8 2. 02	Pounds. 1.5 1.35	Pounds. 2. 6 2. 0	

Although these figures were procured during the progress of regular tests, the conditions outlined in previous reports of the Bureau of Mines indicate clearly that equally good results should be readily obtained in the average commercial producer-gas plant. With this in mind, the following results, reported by the operators and owners of several plants, are of peculiar interest:

Results of operation of producer-gas plants showing fuel consumed per brake horsepower-hour with different fuels.

ANTHRACITE COAL.

Plant No.	Horse- power of each gas	Total horse- power	Heat value of fuel	Fuel fired horsepov	per brake ver-hour.
	generator.	of plant.	as fired.	Rating.	Operating.
			B. t. u.	Pounds.	Pounds.
4	75	150		1.67	
9 6.	300	300 300		1.00 1.25	1.3
6	300 400	400		1. 25	1.3
8	300	600		1, 23	
!•••••••	160	640		1. 25	1.5
4 	250	1,500		1. 20	1.2
Average				1. 26	1.3
ВІ	TUMINOUS	S COAL.			
9	200	200		1. 10	1.0
0	250	250		1.25	
7	200 200	400 400	14,800 14,000	1.25	2.4 1.6
7	250	500	12,520	1.30	1.0
3 	250	500	14,370	1. 20	1.0
7	250	500	14,535	1. 10	
2	500 200	500	14, 770	1.00	1.2
2	K 300	1,000	12,300	1.30	1.4
5	250	1,000	14,835	1. 20	1.0
9	370	1,100	14,500	1.37	1.8
!5 	{ 300 400	1,400		1.10	1.4
	250	1,500		2.80	2.0
8	∫ 375	1,750	13,750	1. 29	1.0
	} 500 500	{	'	1.20	
} 	800	4,200	12,270	1.60	1.2
3 	1,500	6,000	13,740	1.10	1.1
4	1,500	9,000	11,540	. 80	
Average				1.30	1.4
	LIGNIT	E.	<u>' '</u>		<u>'</u>
	100	100	7,440	2, 25	2, 5
, . 	100	100			2.4
8 1	300 200	300 400	11 400		2.0
·L	200	400	11,400	1.50	
Average				· · · · · · · · · · · · · · · · · · ·	2.4
	wooi) .			
3	150	150		4, 00	
26	f 200	} 1,040	5,400	2,50	3.3
	1 280	1,010	, ,,,,,,,,	00	, 0.0

A more direct comparison between the results of commercially operated plants and those obtained at the Government testing station may be had by an inspection of the following tabulation:

Comparative results of operating producer-gas plants by the Government and by commercial companies.

	Fuel consumed per brake horsepower-hour with—											
Operator.	Anthracite.			Bitu	Bituminous coal.			Lignite.			Wooda	
•	Aver- age.	Maxi- mum.	Mini- mum.	Aver- age.	Maxi- mum.	Mini- mum.	Aver- age.	Maxi- mum.	Mini- mum.	Aver-	Average.	
Bureau of Mines Commercial plants	Lbs. 1.3	Lbs. 1.5	Lbs. 1.3	Lbs. 1.3 1.4	Lbs. 2.0 2.4	Lbs. 0.8 1.0	Lbs. 2.0 2.5	Lbs. 2.8 3.0	Lbs. 1.5 2.0	Lbs. 2.6	Lbs. 3.3	

a One sample only used.

Figures showing the heat value of the fuel and the actual consumption of fuel as fired per horsepower-hour for different plants follow:

Heat value of fuel used at different gas producers and fuel consumption per horsepower-hour.

Plant No.	Heat value of fuel.	Fuel fired per horse- power- hour.	Plant No.	Heat value of fuel.	Fuel fired per horse- power- hour.
4	B. t. u. 7,440 11,400 12,270 12,300 13,740 13,750	Pounds. 2.50 3.00 1.20 1.40 1.15 1.00	37. 33. 22. 3. 3.	B. t. u. 14,000 14,370 14,770 14,800 14,835	Pounds. 1. 65 1. 00 1. 20 2. 40 1. 00

It is at once evident that there is no direct relation between the independent results obtained by different operators and the heat value of the fuel used. This lack of relationship is to be expected, as individual plant conditions are so radically different and producergas power is relatively so new that some plants are necessarily much more efficiently operated than others, a fact convincingly borne out by a personal inspection of a large number of plants. Even plants owned by the same corporation, situated in the same district and using the same general grades of fuel, may bear little relation to each other in the results obtained. In one plant after the power used had been changed from steam to producer gas the cost per ton of finished product was reduced to less than one-half of the former cost, whereas in another plant controlled by the same company the cost per ton of finished product was practically doubled after

a similar introduction of producer gas. The difference in the two results seems to have been due to the difference in the methods of the superintendents in charge. One superintendent was a live, wide-awake man who believed it essential to have his power plant kept in perfect condition for the successful manufacture of his product. As a result, he has never shut down for want of power.

The other superintendent felt that the power plant ought to take care of itself. The appearance of the plant testified plainly to his expressed views and serious shutdowns were frequent.

DEPTH OF FUEL BED.

Data supplied by various producer-gas companies regarding the depth of fuel bed used follow:

Data regarding depth of fuel bed used in various producer-gas plants.

PLANTS BURNING ANTHRACITE COAL.

UP-DRAFT PLANTS.

Plant No.	Grate area.	Approxi- mate quan- tity of fuel burned per hour.	Depth of bed.
14	Square feet. 7.1 12.6 13.6 44.2 38.5 38.5 44.2 56.6	Pounds. 125 160 200 300 300 500	Feet. 4 2.5 3 6 2.75 2 10 4
PLANTS BURNING BITUMINOUS	S COAL.		
37	23.7 25.0 50.2 40.0 50.0 50.0 33.1 70.9 78.0 210.0	165 190 300 340 425 435 450 500 680 2,750	2 3 1.5 2.5 2.5 1.75 4 3 1.75 6.5
15	19. 6 41. 3 38. 5	225 350 570	4 2 6.5 1.5
PLANTS BURNING WOOD	•		
13	50. 3 50. 3	605 725	8 7

Data regarding depth of fuel bed used in various producer-gas plants-Continued.

DOWN-DRAFT PLANTS.

PLANTS BURNING BITUMINOUS COAL.

Plant No.	Grate area.	Approxi- mate quan- tity of fuel burned per hour.	Depth of bed.
29	17. 4 17. 4 20. 4	Pounds. 220 250 295 300 625 1,200 1,400	Feet. 5 5 6 12 6 8.5
DOUBLE-ZONE PLANTS.			
PLANT BURNING BITUMINOUS	COAL.		
2	29.3	310	12
PLANT BURNING LIGNITE	c.		
31			8

COMPOSITION OF GAS.

The composition of producer gas varies with the type of producer, the methods and skill used in operating it, the uniformity and regulation of the air and steam supply, the kind and quality of fuel used, the depth of fuel bed, the distribution of the fuel, and the uniformity in size of the fuel. The variations in the composition of producer gas under different operating conditions are readily shown by the following results of analyses of the gas produced in different plants.

Results of analyses of gas from different types of gas producers.

[Results represent per cent by volume.]

UP-DRAFT PLANTS.

PLANTS BURNING ANTHRACITE COAL.

Plant No.	co	CH ₄	C ₂ H ₄	$\mathbf{H_2}$	CO ₂	02	N ₂
14 19	24.0 21.4			12.0 19.0	3.5 7.5	0.2	60.3 51.8
Average	22.7			15.5	5.5	.3	56.0

PLANTS BURNING BITUMINOUS COAL.

37	27. 5 25. 0 21. 8 23. 6 24. 0	2.2 4.3 2.8 4.4 4.6	0.7 .0 .0 .0	6.5 14.6 11.3 14.2 11.6	2.9 5.2 6.4 4.9 4.6	0.2 .9 .4 1.3	60.0 50.0 57.3 51.6 55.2
Average	24.4	3.7	.1	11.6	4.8	.6	54.8

Results of analyses of gas from different types of gas producers—Continued.

UP-DRAFT PLANTS-Continued.

PLANTS BURNING LIGNITE.

P			1	· · · · · · · · · · · · · · · · · · ·	1		1	T
Plant No.		СО	CH4	C_2H_4	H_2	CO_2	O ₂	N_2
38 11 11		16.2 a 21.0 b 9.8	5.0	0.0	25.0	6.9 6.6 16.6	1.3 2.5 3.2	45.
		PLAI	NT BURN	VING WO	OD.			
26		13.6	8.0	0.0	4.0	12.9	0.0	61.
		DOA	VN-DRAE	T PLAN	TS.			
	PLA	NTS BU	RNING I	BITUMIN	OUS COA	L.		
35 8 24		24.0 21.2 25.6	1.6 3.0 .0	0.0 .0 1.0	14.3 9.3 13.6	2. 0 5. 0 5. 0	0.2 .3 .0	57.9 61.2 54.8
Average		23.6	1.5	.3	12.4	4.0	.2	58.0
	· ·	роп	BLE-ZON	IE PLAN	TS.			
	\mathbf{PL}	ANT BUI	RNING B	ITUMINO	US COAI	, .		
8		23.2	2.8	0.0	11.0	6.2	1.1	55.7
		PLAN	r burni	NG LIGN	ITE.			
31		10.4	3.8	0.0	17. 2	15.4	0.4	52.8
		0	IL-GAS	PLANTS.				
	:	PLANTS	BURNIN	G CRUD	E OIL.			
Plant No.	co	CII4	H ₂ S	C_xH_y	H_2	CO_2	O ₂	N ₂
10	10. 2 7. 4	6. 1 12. 7	0.0 3.1	3.8 2.6	10.6	6.1 4.5	0.0	63.2 69.3

a No steam.

b With steam.

The averages of several typical analyses of producer gas from the Bureau of Mines testing plant and the averages of the figures presented for plants in commercial operation are given below. Attention is called to the fact that the analyses may not be strictly comparable, because methods of analyses may have differed slightly.

Average results of analyses of producer gas from Bureau of Mines testing plants and from commercial plants.

[Results represent per cent by volume.] UP-DRAFT PLANTS.

	Gas from anthracite coal.		Gas from bitu- minous coal.		Gas from lignite.		Gasfroi	n peat.a	Gasfrom wood.a	
Constituent.	Bureau of Mines.	Com- mercial plants.	Bureau of Mines.	Com- mercial plants.	Bureau of Mines.	Com- mercial plants.	Bureau of Mines.	Com- mercial plants.	Bureau of Mines.	Com- mercial plants.
Carbon monoxide (CO)		.0 .0 15.5 5.5	18. 28 3. 12 . 18 12. 90 9. 84 . 04 55. 64	24.4 3.7 .1 11.6 4.8 .6 54.8	21.00 2.20 .40 18.50 12.40 .00 45.50		21.0 2.2 .4 18.5 12.4 .0 45.5			13.6 8.0 .0 4.0 12.9 .0 61.7

a One sample only.

DOWN-DRAFT PLANTS.

		from ite coal.	Gas fro minou	m bitu- s coal.	Gasfron	n lignite.	Gasfro	m peat.	Gasfro	m wood.
Constituent.	Bureau of Mines.	Com- mercial plants.	Bureau of Mines.	mercial	Bureau of Mines.	Com- mercial plants.	Bureau of Mines.	Com- mercial plants.	Bureau of Mines.	Com- mercial plants.
Carbon monoxide (CO) Methane (CH ₄) Ethylene (C ₂ H ₄) Hydrogen (H ₂). Carbon dioxide(CO ₂) Oxygen (O ₂). Nitrogen (N ₂)			1.1 .0 11.4 7.6 .2	23.6 1.5 .3 12.4 4.0 .2 58.0	1.7 .0 13.3 11.5		1.5 .1 13.3 12.9			

HEAT VALUE OF GAS.

Figures showing the heat value of the gas from different fuels determined from the average of a large number of tests reported by the Bureau of Mines and also from the figures submitted by the operators of plants in commercial operation are presented below:

Average heat values of gas from different fuels when used in various types of gas producers.

[Figures represent British thermal units per cubic foot of gas.]

UP-DRAFT PLANTS.

Location of gas pro-			Gas from bituminous coal.		Gas from lignite.		Gas from peat.		Gas from wood.	
ducer.	Average.	Maxi- mum.	Aver- age.	Maxi- mum.	Average.	Maxi- mum.	Aver- age.	Maxi- mum.	Aver- age.	Maxi- mum.
Bureau of mines testing station Commercial plants	138		152 151	176 175	158 157	188 185	a 175		a 133	

a One sample only.

Average heat values of gas from different fuels when used in various types of gas producers—Continued.

DOWN-DRAFT PLANTS.

Location of gas pro-		om an- te coal.	Gas from bitu- minous coal.		Gas from	n lignite.	Gas fro	m peat.	Gas fro	m wood.
ducer.	Aver- age.	ge. mum. age. mum. age. mum. age. mum. 110 123 111 127 4115 4119	Aver- age.	Maxi- mum.						
Bureau of mines testing station			110 123	123 130	111	127	a 115	a 119		
			DOUBL	E-ZON	E PLAN	ITS.				
Bureau of mines testing station Commercial plants			(p)		118					
			OIL	-GAS P	LANTS.					
Bureau of mines testing station				c 215	c 230					

CUBIC FEET OF GAS PER POUND OF FUEL.

Tabulated data showing the quantity of producer gas available from various fuels used in the different types of plants follow:

Average quantities of gas produced from different fuels in different types of gas producers.

[Figures represent cubic feet of standard (60° F. and 30 inches of mercury) gas per pound of fuel.]

UP-DRAFT PLANTS.

	Gas from bituminous coal.				Gas from lignite.				Gas from peat.			
Location of gas producer.	As fired.		Dry.		As fired.		Dry.		As fired.		Dry.	
	Aver- age.	Maxi- mum.		Maxi- mum.		Maxi- mum.		Maxi- mum.				Maxi- mum.
Bureau of mines testing station	61 75	101 96	65	104	36	46	46	53	a 30		a 38	

a One sample only.

43186°—Bull. 109—16——3

a Two samples only. $\mathfrak b$ Tests indicate this figure to be approximately 115. $\mathfrak c$ Figures represent two plants burning crude oil.

b Two samples only.

TIME BETWEEN FUEL CHARGES AND WEIGHT OF FUEL CHARGES.

Figures showing the time between fuel charges and the weight of fuel charges in the various types of plants follow:

Time between fuel charges and weight of fuel charges in different types of gas producers.

UP-DRAFT PLANTS.

PLANTS BURNING ANTHRACITE COAL.

Plant No.	Horsepower of each gas generator.	Average fuel burned per hour.	Length of service per day.	Time be- tween fuel charges.	Weight of fuel charge.
6932	150 160 250 300 300 300 350	Pounds. 160 190 300 200	Hours. 24 24 3 to 7 11 24 10 5 to 24	Hours. 1 to 6 .5 2 24 6 10 .5	Pounds. 200 200 to 600 1,800 to 2,400 1,000 to 1,500 2,000 175
PLANTS BU	RNING BI	ruminous	COAL.		
3	200 200 250 250 370 650 1,000 2,500	190 165 450 215 300 435 680 2,750	24 10 14 24 } 10 24	1 .5 4 .75 .17 .13 2.5	165 80 1,500 250 100 100 7,000
PLANTS	BURNING	3 LIGNITE			
4	100 100 100 250 300	225 175 570 350	8 11 14 24 24	$\begin{array}{c} 2 \\ 1 \\ 2 \text{ to } 3 \\ 2 \text{ to } 3 \end{array}$	500 to 800 175 200 to 300 190 900
PLAN	T BURNII	NG WOOD.			
26	{ 200 280	}	24	0.5	280
DOV	N-DRAFT	PLANTS.			'
PLANTS BU	RNING BI	ruminous	COAL.		
29	200 250 250 250 375 500 800 1,500	295 300 625 1,200 1,400	24 10 10 24 24 24	0.5 .25 .17 .17 .25 .09	110 50 50 100
DOU. PLANT BUF	BLE-ZONE	-	COAL		
2	250	310	24	1 to 1.5	

TIME BETWEEN POKINGS OF FUEL BED.

Tabulated data showing the time between pokings of the fuel bed in the various types of plants are presented below:

Time between pokings of fuel bed in different types of gas producers.

UP-DRAFT PLANTS.

PLANTS BURNING ANTHRACITE COAL.

Plant No.	Area of fuel bed.	Depth of fuel bed.	Approximate amount of fuel burned	Time between
			per hour.	pokings.
14	Square feet. 7. 1 12. 6 13. 6 44. 2 38. 5 44. 2 56. 6	Feet. 4 2.5 3 6 2 10	Pounds. 125 160 200 300 300 500	Hours. 1 .75 3 to 6 10 1 8 1 6
PLANTS BURNING BI	ruminous	COAL.		
37. 3. 25. 21. 17. 33. 5. 21.	23. 7 25. 0 40. 0 50. 0 33. 1 28. 3 70. 9 78. 0 210	2 3 2. 5 1. 75 4 3 1. 75 6. 5	165 190 340 435 450 215 500 680 2,750	10 .33 4 .75 1 2 1 .75
PLANTS BURNIN	G LIGNIT	€.		
15. 7. 4.	20. 4 19. 6 38. 5	4 2 1. 5	175 225 570	1 12 2 12
PLANTS BURNI	NG WOOD			
13	50. 3 50. 3	8 7	605 725	0. 25 . 16
DOWN-DRAFT		COLT		
PLANTS BURNING BI		COAL.	1	
29 22 27 35 8 23	17. 4 17. 4 20. 4 36. 0 60. 0	5 6 12 8.5 9	220 250 295 300 1,200 1,400	(a) $.5 to 1$ (a) (a)
DOUBLE-ZONE		00.17		
PLANT BURNING BIT	ruminous	COAL.		
2	29.3	12	310	1
				-
PLANT BURNIN	G LIGNITE	E.		

a Not poked.

TROUBLE FROM HOLES AND CHANNELS IN FUEL.

Data supplied by owners or operators regarding trouble from holes and channels in the fuel bed in the various types of plants are presented below. The numbers preceding each paragraph refer to plant numbers assigned by the author:

Data regarding holes and channels in full bed.

UP-DRAFT PLANTS.

Plants burning anthracite coal.

1. Causes back-firing trouble.

6. Little trouble from holes and channels.

9. Little trouble, because we use sufficient producer capacity. 14. Not serious. Holes easily closed.

16. Considerable stoking required at times.

19. No trouble.

20. Permit gas to burn in producer.

32. Shut the engine down.

34. Make weak gas. 36. No trouble.

Plants burning bituminous coal.

3. Cause poor gas and clinker.5. Little trouble.

12. No trouble when producers have proper attention.

17. No trouble.

21. Cause much trouble.

- 25. No trouble.
 33. Not appreciable.
- 37. Cause weak gas.
 39. Serious. Necessitating laborious work to keep the fire even throughout the bed.

Plants burning lignite.

4. Occasional, but never serious.

7. Destroys gas.

 No trouble. Dropping fuel on fire keeps it down.
 Very little. Never have this trouble, as little work keeps the fuel bed in fine shape.

Plants burning wood.

- 13. Permit unfixed oxygen to reach top of fuel bed, causing burning.
- 26. No trouble.

DOWN-DRAFT PLANTS.

Plants burning bituminous coal.

No trouble.

20. Permits gas to burn in producer.

22. No trouble.

- 23. Do not let them occur.
- Readily noticeable on recording calorimeter. Believed to have affected results seriously.
 - 27. Fire must be closely watched and fuel charged lightly.

28. No trouble.

29. Considerable. At times had to shut plant down.

No trouble.

DOUBLE-ZONE PLANTS.

Plants burning bituminous coal.

- Quite serious.
 No trouble.

METHODS OF OVERCOMING VARIATIONS IN QUALITY OF GAS.

Data supplied by owners or operators regarding methods of overcoming variations in the quality of the gas yielded by the various types of gas producers follow:

Data regarding methods used for overcoming variations in gas quality in various types of gas producers.

UP-DRAFT PLANTS. PLANTS BURNING ANTHRACITE COAL.

Plant No. Horsepower of each gas generator. Remarks of owner or operator regarding methods used to overco tions in quality of gas.	me varia-
14 75 None.	
6 150 Variation of steam feed.	
9 160 None.	
20 200 Suction producer, none; pressure producer, gasometer.	
32 250 Change setting of mixing valve on engine.	
19 300 Automatic vapor control and proper cleaning methods.	
36 300 Automatically controlling steam supply to producer.	
16 400 Producer automatically regulated.	
PLANTS BURNING BITUMINOUS COAL.	
000 0 111	
3 200 Gas holder.	
37 200 By keeping fires regular gas quality varies but very little. 17 250 None.	
33 250 None.	
39 370 None, except best possible attention to producer fuel bed.	
25 300, 400 Hand regulation of air temperature admitted to ash bed.	
21 650, 1,000 None, except to reprimand gasmen.	
5 1,000 Keep bed tight, uniform, and free from air pockets.	
12 200, 300, 2, 500 Gas quality checked by recording calorimeter.	
PLANTS BURNING LIGNITE.	
4 100 Change mixture at engine.	
7 100 Adjustment of levers.	
15 100 More or less free air.	
11 250 Mixing valves on engines. Gas constant except when cleaning fi	res.
38 None. Little variation.	
PLANT BURNING WOOD.	
26 200, 280 None.	
DOWN-DRAFT PLANTS.	
PLANTS BURNING BITUMINOUS COAL.	
20 00 00 00 00	
29 200 Close attention to fire.	
35 250 Keep fires and scrubbers clean. 28 375, 500 20,000-cubic foot gas holder.	
22 500 None, except with fires in generators and mixing in gas holders.	
8 800 Water gas run to regulate temperature of fires.	
23 1,500 None other than holder.	
24 1,500 Mixture of gas from different producers. Careful watching of fire	es.
DOUBLE-ZONE PLANTS.	
PLANT BURNING BITUMINOUS COAL.	
0	
2 250 None.	

Data regarding methods used for overcoming variations in gas quality in various types of gas producers—Continued.

DOUBLE-ZONE PLANTS-Continued.

PLANT BURNING LIGNITE.

Plant No.	Horsepower of each gas generator.	Remarks of owner or operator regarding methods used to overcome variations in quality of gas.
31	200	Change mixing valves on engine.

OIL-GAS PLANT.

PLANT BURNING CRUDE OIL.

10	400	Variations so slight that governor handles them easily.

METHODS OF CLEANING GAS GENERATORS.

The owners and operators of producer-gas plants were asked to describe briefly their method of cleaning the gas generator; they were requested to state the time and the number of men required for cleaning each unit. Brief abstracts of the replies received are tabulated below.

Data regarding methods of cleaning gas generators in various types of producer-gas plants.

UP-DRAFT PLANTS. PLANTS BURNING ANTHRACITE.

Plant No.	Horse- power of each gas generator.	Total horse- power of plant.	Remarks of owner or operator regarding methods used to clean gas generator.
		150	
14	75	150	Coal and ash pulled through doors above grate; clinkers removed from walls by bar through poke hole; 3 hours' time of 1 man.
6	150	450	Half close valve between producer and gas main; remove all ashes be- tween grates and fire with hoe and poker; poke fire down and a d d fresh fuel: 1 hour's time of 1 man.
9	160	640	Draw ash and clinker, allowing fire to settle down to grate; one-half hour's time of 1 man.
32	250	500	After shutting down at 6 p. m., ashes raked out at water seal; 1 hour's time of 1 man.
19	300	300	Ash removed from center of fire by rocking grate operated by com- pressed-air cylinder; fine ash is barred from lining and raked out; 2 hours' time of 1 man.
36	300	300	Bar lining; shake grate; 1 hour's time of 1 man.
1	350	700	Raked out from bottom; 2 to 3 hours' time of 2 men.
16	400	400	Ash is taken out at two intervals in 24 hours; 1 to 2 hours' time of 1 man.

		PL	ANTS BURNING BITUMINOUS COAL.
3	200	400	Air and steam cut off for a couple of days; ash and coal removed through water seal; 3 hours' time of 1 man.
37	200	400	All free ash is removed from bed, leaving fire bridged; bed is then broken down and producer filled; $1\frac{1}{2}$ hours' time of 2 men.
17	250	500	Shaking the grates and pulling the ashes; three-fourths of an hour's time of 1 man.
39	370	1,100	Remove sufficient ash from water seal to let bed down to normal level; work loose bed down to new level with poke bars; break clinkers off walls and smash fine with chisel bars and heavy hammers; 12 hours' time of 3 men is the minimum.
25	300 400	1,400	(a) Clean by hand-operated rotary table; (b) clean by air-driven shaking grate; 5 minutes' time of 1 man; clean when running.
21 5	650, 1, 000	3,650	Not much of this to do.
5	1,000	4,000	Draw ashes till bed drops 1 foot; poke fire till solid; 1½ hours' time of 1 man.
12	2,500	2,500	Twenty minutes to 1 hour's time of 1 man.

 $\label{lem:continued} Data\,regarding\,methods\,of\,cleaning\,gas\,generators\,in\,various\,types\,of\,producer\text{-}gas\,plants\text{--}\\ \text{Continued}.$

UP-DRAFT PLANTS—Continued.

PLANTS BURNING LIGNITE.

			PLANTS BURNING LIGHTE.	
Plant No. Horse-power of each gas generator. Horse-power of each gas generator. Remarks of owner or operator regarding methods used to generator.				
4	100	100	Burn low; rake and clean everything out; 6 hours' time of 2 men.	
15 11	100 250	100 500	If run 3 days, 24 hours per day, take out everything; if run 14 hours a day, clean every day; for 3 days' run, 3 hours' time of 1 man. Bar fires, and take out ashes, working around producer several times to prevent fire dropping; if gas becomes weak, stop a while; 1½ hours'	
38	300	300	time of 2 men. Run fuel bed down till 3 or 4 feet deep; open hoppers and all poke holes and draw out fire below; fire is kindled by layer of shavings and fine wood on grates about 12 inches deep; cover with layer of 4 inches of good dry coal; after well lighted, fill with coal; close hoppers and poke holes, starting gas washer for draft; 10 hours' time of 2 or 3 men.	
			PLANTS BURNING WOOD.	
13	150	150	Producer cleaned daily by removal of ashes; scrubber pit cleaned every	
26	200, 280	1,040	hour or so to avoid tar clogging the main; work done by 1 man. Beds lowered by removing ash once a month through water seal; 3 hours' time of 2 men.	
	ı	ı	NTS BURNING BITUMINOUS COAL.	
	200	200	Dig out from bottom and punch down from top; 15 minutes' time of 1	
27	250	500	l man	
			Let producer stand from Saturday till Monday; spray fire with water on top for 15 minutes; let stand for 1 hour; clean everything out; recharge with 2,000 pounds of coke; 10 hours' time of 2 men. Fuel and ash are cleaned out every 2 weeks and new fires started; 4	
35	i	1,000	hours' time of 6 men.	
28	1	1,750	Clinker sometimes very hard and must be broken with bar from above; 6 to 10 hours' time of 8 men for each pair of producers. All ash, refuse, and clinkers removed; 5 hours' time of 3 men.	
8	800	3,200	Set is cut out; cooled with water; ashes removed; clinker cut down; 8 hours' time of 4 men.	
23		6,000	Water sprayed through charging door directly after run till fire is cooled;	
24	1,500	9,000	Power-gas producer: Put fire out; remove clinker, coke, and ash; 2 to 4 days' time of 3 to 5 men. Heating gas producer: Throw fire to one side; clean grate; throw fire back; repeat for other side; 1 to 2 hours' time of 1 man.	
		•	DOUBLE-ZONE PLANTS.	
		PLA	ANTS BURNING BITUMINOUS COAL.	
2 8	250 500	250 500	Not necessary to shut down to clean. See procedure under "' Down-draft plants."	
			OIL-GAS PLANT.	
			PLANT BURNING CRUDE OIL.	
30			Raise stack valve, shut off blower, remove coke, close door, turn on blast, adjust oil, and lower stack; 10 minutes' time of 1 man.	

SERIOUS CLEANING TROUBLES.

Data furnished by owners and operators regarding cleaning troubles in the different types of gas producers are presented in the tabulation following:

Data regarding cleaning troubles in various types of gas producers.

UP-DRAFT PLANTS. PLANTS BURNING ANTHRACITE COAL.

Plant No.	Horsepower of each gas generator.	Total horse- power of plant.	Remarks of owner or operator regarding cleaning troubles.		
14 6 9 32 19	75 150 160 250 300 400	150 450 640 500 300 400	None. None. Only care is to guard against too much intake air. Not to allow ashes and clinker to work up along walls. None. None.		
16	400	400	Taking out too many ashes, allowing bed to drop too low.		
		PLA	NTS BURNING BITUMINOUS COAL.		
3 37	200 200	400 400	Little trouble. If bed hangs it may burn man in falling. Occasional difficulty in breaking down the bridge; then must drive the		
39	370	1,100	bar through with the sledge. Impossibility of properly breaking up and settling clinker so as to main- tain even fire.		
5 12	1,000 2,500	4,000 2,500	None. None.		
		<u>.</u>	PLANTS BURNING LIGNITE.		
15 11 38	100 250 300	100 500 300	Clinker. None unless fire is allowed to drop. None. Same lining in producer for 5 years. Cleaning out hard mixture of tar and ash deposit in gas collector and scrubber inlet pipe is dirty work and takes a little time.		
			PLANTS BURNING WOOD.		
13 26	150 200, 280	150 1,040	Filling of gas main by tar. This is burned out occasionally. To be done away with by improved gas cleaner. Tar.		
		<u> </u>	DOWN-DRAFT PLANTS.		
		PLA	NTS BURNING BITUMINOUS COAL.		
29 27 35 28 22 8 23 24	200 250 250 375, 500 500 800 1, 500	200 500 1,000 1,750 500 3,200 6,000 9,000	Poor gas and sometimes trouble with clinkers. Producer can not be cleaned while running. Heat and dirt. Hard clinker. Chopping down clinker. None. None. Hard clinker Loss of coke and thin fire to start next run.		
		'	DOUBLE-ZONE PLANT.		
		PLANT	BURNING BITUMINOUS COAL.		
8	500	500	None.		
			OIL-GAS PLANT. PLANT BURNING CRUDE OIL.		
30	•••••		The rapidity with which generator must be cleaned. Reserve gas supply limited.		

TIME BETWEEN PERIODS OF DRAWING PRODUCER FIRES.

The following tabulation gives data regarding time between periods of drawing producer fires in the various types of gas producers:

Data regarding time between periods of drawing producer fires in various types of gas producers.

UP-DRAFT PLANTS.PLANTS BURNING ANTHRACITE COAL.

	1 1111	NTS BURNING ANTHRACITE COAL.	
Horsepower of each gas generator.	Total horsepower of plant.	Remarks of owner or operator regarding time between periods of drawing producer fires.	
75 200 250 300 300 350 400	500 300 300 700 400	20 days. 45 days. Present fire, 8 months; previous fire, 4 years. Once a year. Indefinite. 14 days. One producer each week. Not drawn.	
	PLA	NTS BURNING BITUMINOUS COAL.	
200 200 250 370 650, 1, 000 1, 000 2, 500	1,100 3,650 4,000 2,500	365 days. 10 days. 2 days. Fires not drawn except for repairs. 12 months. Every third day. 6 months to 1 year.	
	i	PLANT BURNING LIGNITE.	
100 300	100 300	120 days. About once a year.	
	<u>'</u>	PLANT BURNING WOOD.	
200, 280	1,040	3 months or more.	
		DOWN-DRAFT PLANTS.	
	PLA	ANTS BURNING BITUMINOUS COAL.	
200 250 250 250 375, 500 500 800 1, 500 1, 500	200 500 1,000 1,750 500 3,200 6,000 9,000	3 months. 45 days. 6 days; necessary to cut unit out when coke is 80 to 90 per cent burned out and producer badly clinkered. 12 days. 14 days. Weekly. 10 to 15 days. 13 to 17 days. 15 to 21 days.	
DOUBLE-ZONE PLANTS. PLANTS BURNING BITUMINOUS COAL.			
250 500	250 500	Do not draw fires. 10 to 15 days.	
		PLANT BURNING LIGNITE.	
200		2 years.	
		OIL-GAS PLANT. PLANT BURNING CRUDE OIL.	
		Every 8 hours.	
	200 250 250 250 250 250 250 1,500 1,500 1,500 1,500 1,500 1,500	Horsepower of each gas generator. Total orsepower of plant. Total orsepower generator. 150	

METHODS OF SCRUBBING AND CLEANING GAS.

Data supplied by owners and operators regarding methods of scrubbing and cleaning the gas in the various types of gas producers follow.

Data regarding methods of scrubbing and cleaning gas in various types of gas producers.

UP-DRAFT PLANTS.

PLANTS BURNING ANTHRACITE.

		PLANTS BURNING ANTHRACITE.
Plant No.	Horse- power of each gas generator.	Replies from owners or operators.
6 20 34 19 36 1	150 200 250 300 300 350 400	Counter flow wet coke tower scrubber and excelsior dry scrubber. Coke. Water spray dripped through coke. Static washer. Static scrubber. Centrifugal tar extractor. Wood cross sections through which water flows. Coke between 1 and 2 inches with water sprays.
		PLANTS BURNING BITUMINOUS COAL.
3 37 17 33 39 25 21 5	650, 1, 000	Latticed spray scrubbers, rotary tar extractors and purifiers. Rotary water-jet scrubber. Smith type "F" tar extractors connected in series. Preliminary wet scrubber, counter current. Rotary scrubber and dry scrubber. Cooled in first pass of wet scrubber, passed through wooden checker work which is sprayed with water. Passed through centrifugal tar extractor to holder. Cooling, spraying, and tar extracting. Wood centrifugal tar extractor on one plant and Smith static tar extractor on the other. Saaler washers. Four coolers with water spray. No filling in coolers. Buffalo scrubber. No dry scrubber used. Gas for heating purposes and not for engines. Smith type "F" spun-glass tar extractors.
<u> </u>	<u> </u>	PLANTS BURNING LIGNITE.
	1	
4 11	100 250	Cooling with water and passing through mechanical scrubber. Gas passes through baffles of 2-inch by 4-inch timbers placed on edge, set close together, 14 feet high. Four streams of water flush each scrubber. Gas then passes through tar extractor.
38	300	Spray scrubber and mechanical gas washer (tar extractor).
		PLANTS BURNING WOOD.
26	200, 280	Static scrubber, centrifugal tar extractor.
		DOWN-DRAFT PLANTS.
		PLANTS BURNING BITUMINOUS COAL.
29	200	Cooled with water spray. Passed through coke with water running over it and down through 6 or 8 feet of straw.
27	250	Scrubbers, 28 inches in diameter by 14 feet, each with seven water sprays. Each exhauster has 16 sprays, throwing water at 40 pounds' pressure against first impeller running at 3,500 revolutions per minute.
35 28 22 8 23	375, 500 500 800 1, 500	peller running at 3,500 revolutions per minute. Passed through wet and dry scrubber, coke and excelsior. Passed through wet scrubber and then exhauster and dry scrubber. One wet scrubber filled with excelsior, other with coke. Both dry scrubbers filled with excelsior. Cooling in boiler, wet scrubber and dry scrubber. Static wet scrubbers with water sprays, dry scrubber with excelsior. Gas runs down center of cooler through spray, up inside of shell, through sprays and through a rotary scrubber. Plant A—through vertical boiler, spray cooler, and centrifugal scrubber. Plant B—gas is not clean except from one producer. Special use. Cooled centrifugal tar scrubber and dry cleaner.

Data regarding methods of scrubbing and cleaning gas in various types of gas producers— Continued.

DOUBLE-ZONE PLANTS.

PLANTS BURNING BITUMINOUS COAL.

Plant No.	Horse- power of each gas generator.	Replies from owners or operators.		
2 8	250 500			
		PLANT BURNING LIGNITE.		
31	200	200 Water spray.		
		OIL-GAS PLANTS.		
		PLANTS BURNING CRUDE OIL		
10	400	falo Forge centrifugal scrubber cleaning to about 0.02 grain per cubic foot. Used 2		
30		years without sign of need of change. Gas is forced through three turns, 10 inches by 18 feet, against a gravity flow of water running over baffle plates.		

TIME BETWEEN RENEWALS OF SCRUBBER MATERIAL.

The owners and operators questioned furnished little information relating to the time between changes in the scrubber material used in the producer-gas installations. The few plants that reported indicated the periods to be as follows:

Time between renewals of scrubber material in various types of producer-gas plants.

UP-DRAFT PLANTS.

Plants hurning anthrocita coal

	riants burning anthrac	
Plant No.		Time between renewals of scrubber material, months.
20		
16		
6		$\int_a^a 24 \text{ to } 36$
0		$ \begin{cases} a & 24 \text{ to } 36 \\ b & 3 \text{ to } 6 \end{cases} $
9		6
34		
	Plants burning bitumin	ous coal.
33		8
12		2 to 5
21		3
	Plant burning lign	ite.
11		Never.
	Plant burning woo	
26		Never.
	a Coke.	b Excelsior.

DOWN-DRAFT PLANTS.

	Plants burning bi	tuminous coal.	
Plant No.	_		Time between renewals of scrubber material, months.
29		. 	6 to 12
00			\b 0.5
22			∫ ^c 2
8			11
24			1 to $1\frac{1}{2}$
	b Excelsion		_

OPINIONS REGARDING SCRUBBING AND CLEANING RESULTS.

The various owners and operators were asked whether the scrubbing and cleaning results in their producers were satisfactory, and if not, why. The data obtained on this point are presented below:

Data regarding satisfactoriness of scrubbing and cleaning results in various types of gas producers.

UP-DRAFT PLANTS.PLANTS BURNING ANTHRACITE.

	Thirtie Berning Milmitelli.				
Plant No.	Horsepower of each gas generator.	Remarks of owner or operator regarding satisfactoriness of scrubbing and cleaning results.			
6 9	160 Do. 200 Do. 250 Do. 250 Do. 300 Do. 300 Do. 300 Fairly.				
	PLANTS BURNING BITUMINOUS COAL.				
3	250 370 300,400	Satisfactory. Very satisfactory. Not satisfactory. Considerable tar remains in gas and clogs engine valves. As satisfactory as ever observed in pressure up-draft producer using bituminous coal. Satisfactory. Does very well, though gas carries tar after cleaning. For heating purposes; not for gas engines. Entirely satisfactory.			
		PLANTS BURNING LIGNITE.			
4 7 11 38	100 100 250 300	Satisfactory. Do. Satisfactory. Tar gives no trouble whatever in engine. Satisfactory. Except occasional cleaning each 3 to 4 months. Tar is of soft paraffin nature, but contains a resinal substance, and when dry is hard to remove.			
		PLANTS BURNING WOOD.			
13 26	150 200,280	Not satisfactory. Are preparing more complete arrangements to recover acids and tars for utilization and for elimination of condensed matter in gas mains. Not satisfactory. On account of moisture and tar.			

 $\begin{tabular}{lll} Data\ regarding\ satisfactoriness\ of\ scrubbing\ and\ cleaning\ results\ in\ various\ types\ of\ gas\ producers$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$

DOWN-DRAFT PLANTS.

PLANTS BURNING BITUMINOUS COAL.

Plant No.	Horsepower of each gas generator.	Remarks of owner or operator regarding satisfactoriness of scrubbing and cleaning results.			
29 27 35 28 22 8 23 24	200 250 250 250 375,500 500 800 1,500 1,500	Does not remove lampblack. Not satisfactory. Considerable dirt and dust get by. Pipes have to be cleaned out occasionally. Not entirely satisfactory. Soot and lampblack not completely removed. Satisfactory. Discrept Satisfactory.			
	DOUBLE-ZONE PLANTS.				
		PLANTS BURNING BITUMINOUS COAL.			
2 8	. 250 Not satisfactory. Does not remove tar. Satisfactory.				
	PLANT BURNING LIGNITE.				
31	200	Satisfactory.			
		OIL-GAS PLANTS.			
		PLANTS BURNING CRUDE OIL.			
10	400	No tar. Not satisfactory. Very difficult to get out the floating carbon.			

MANNER IN WHICH TAR GIVES TROUBLE.

Data obtained from the operators and owners in response to a query as to the way in which tar gave trouble are presented in the tabulation following:

Data regarding tar troubles in various types of gas producers.

UP-DRAFT PLANTS.

PLANTS BURNING BITUMINOUS COAL.

Plant No.	Horse- power of each gas generator.	Statement of owner or operator regarding tar troubles.
3 37 33 39	200 200 250 370	No operating trouble. Clogs the governor valve on engine. Choking and sticking of engine valve. Clogs mains, fitings, engine regulators, and inlet valve passages. Frequent cleaning of all gas piping required.
25 21 5	$ \begin{cases} 300,400 \\ 650,1,000 \\ 1,000 \\ 200 \\ 300 \\ 2,500 \end{cases} $	No trouble. No trouble where gas is used. Most in gas house in handling. Have little trouble where gas is used. Chokes pipes between cooling tower and washers. No trouble at all.

Data regarding tar troubles in various types of gas producers—Continued.

UP-DRAFT PLANTS—Continued.

PLANTS BURNING LIGNITE.

Plant No.	Horse- power of each gas generator	ower of sach gas Statement of owner or operator regarding tar troubles.	
4 11 38	250		
		PLANTS BURNING WOOD.	
13 26	150 Clogging mains. 200,280 In long gas lines to engine and admission valves.		

DOWN-DRAFT PLANTS.

PLANTS BURNING BITUMINOUS COAL.

29 27 35 28 8 23 24	250 250 375,500 800	Makes engine valve stick and causes some trouble in exhauster. Produced only when starting new fire. Clogs ports in exhauster. Clogs scrubbers. No trouble. Do. Do. Labor for cleaning water seal, stopping sprays in cooler and scrubber. Small amount collects at burners in few months, interfering with the seating of mushroom valves on the line.
---------------------------------------	------------------------------	---

DOUBLE-ZONE PLANTS.

PLANTS BURNING BITUMINOUS COAL.

2 8	250 500	Sticking intake valves. No trouble.		
		PLANT BURNING LIGNITE.		
31	200	On valves of engines.		

OIL-GAS PLANT.

PLANT BURNING CRUDE OIL.

30 Causes throttle, poppet, and inlet valves and stack to choke.
--

TROUBLE CAUSED BY LAMPBLACK.

Data supplied by owners and operators regarding trouble caused by lampblack follow:

Data regarding trouble from lampblack in various types of producers.

UP-DRAFT PLANTS.

PLANTS BURNING BITUMINOUS COAL.

Plant No.	Horsepower of each gas generator	Remarks of owner or operator regarding trouble caused by lampblack.
3 37 33 39 25 21	200 200 250 370 300, 400 650, 1,000 200, 300, 2,500	Stops water outlet in spray scrubbers. By collecting in and reducing area of gas mains. Lampblack mixing with tar. No trouble observed. If any, it is mixed with tar. No trouble. Choking flues in producers and coolers. No trouble.

DOWN-DRAFT PLANTS.

PLANTS BURNING BITUMINOUS COAL.

27 35 28 22 8 24	375, 500 500 800	Mixes with oil and gums engine valves. Clogs scrubbers. Deposits in pipes. In engine cylinder. Deposits on inlet valves. No trouble. Do.
---------------------------------	------------------------	--

DOUBLE-ZONE PLANT.

PLANT BURNING BITUMINOUS COAL.

8	800	No trouble.

OIL-GAS PLANTS.

PLANTS BURNING CRUDE OIL.

10	400	Gradually chokes gas line and soots up gas valves. Requires cleaning every 6 months; 10-hour job.
30		Clogs gas main. Works by piston rings and mixes with lubricating oil.

RELATION OF TAR OR LAMPBLACK IN ENGINE TO COST OF LUBRICATION.

In response to a query as to whether the cost of engine lubrication is materially increased by the presence of tar or lampblack in the engine, the following information was supplied:

Data regarding relation of lampblack in gas-producer engine to cost of lubrication.

UP-DRAFT PLANTS.

PLANT BURNING ANTHRACITE COAL.

Plant No.	Horsepower of each gas generator.	Remarks of owner or operator in response to the query: "Is the cost of engine lubrication increased by the presence of tar or lampblack?"			
9	160	No.			
		PLANTS BURNING BITUMINOUS COAL.			
3 33 39 25 21 5	200 250 370 300, 400 650, 1,000 1,000	No. Yes. Not determined. No. Not greatly. Yes.			
		PLANT BURNING LIGNITE.			
4	100	No.			
		PLANT BURNING WOOD.			
26	200, 280	Yes.			
		DOWN-DRAFT PLANTS. PLANTS BURNING BITUMINOUS COAL.			
29 22 8 23 24	200 500 800 1,500 1,500	No. Not materially. No. Yes. Think not.			
		PLANT BURNING LIGNITE.			
38	300	No. No lampblack ever seen.			
		DOUBLE-ZONE PLANTS. PLANTS BURNING BITUMINOUS COAL.			
2 8	250 500	No. Do.			
		PLANT BURNING LIGNITE.			
31	200	Yes.			
		OIL-GAS PLANTS. PLANTS BURNING CRUDE OIL.			
10	400	No. No. Use cheap oil.			

BURNER TROUBLE CAUSED BY TAR AND LAMPBLACK.

Data supplied by owners and operators regarding trouble from tar or lampblack clogging the gas burners in the various types of gas producers follow; the number at the beginning of each paragraph indicates the plant that supplied the information:

- 5. None.
- 9. None.
- 12. None.
- 13. Burner is piece of 8-inch iron pipe; clogged sometimes; cleaned once per month.
 - 17. Latest burner gives no trouble.
 - 22. None.
 - 24. No trouble. Remove some lump tar from burners about once each two months.
 - 25. Gas so cleaned that no trouble is experienced.
 - 30. None.
 - 32. None.
 - 35. Burners clog.
 - 38. None.

TROUBLE FROM SULPHUR IN PRODUCER GAS.

Data regarding trouble from sulphur in producer gas as experienced by the various owners and operators follow:

Data regarding trouble from sulphur in gas of various types of gas producers.

UP-DRAFT PLANTS.
PLANTS BURNING ANTHRACITE COAL.

		FLANIS BURNING ANTIRACITE COAL.
Plant No.	Horsepower of each gas generator.	Replies from owners or operators.
9 20 18	160 200 300 300	None. Do. Trouble; by clogging passages where velocity of flow is changed and by eating out sheet-steel parts. None.
		PLANTS BURNING BITUMINOUS COAL.
3 37 17 25 21 5	200 200 250 300, 400 650, 1,000 1,000 2,500	Cuts water-cooled valves. None. When producer has stood over for 20 hours sulphur is noticed by men at furnaces. None. Trouble, Trouble; causes distress among employees. Trouble; high sulphur gives unpleasant fumes in factory.
		PLANTS BURNING LIGNITE.
11 38	250 300	Exhaust valve seats become pitted. None, except that engine exhaust has deteriorated roof metal work, guy ropes, etc.
		DOWN-DRAFT PLANTS.
		PLANTS BURNING BITUMINOUS COAL.
29 20 35 28 22 8 23 24	200 250 250 250 375, 500 500 800 1,500	None. Do. Do. Do. Do. Trouble; acts on valves and pipes, and particularly on exhaust. No serious trouble. None. Do.

PROPORTION OF SULPHUR ALLOWABLE IN FUEL.

The owners and operators were asked as to what percentage of sulphur could be present in the gas-producer fuel without causing inconvenience to the workmen. Summarized data supplied in the replies follow:

Data regarding percentage of sulphur allowable in fuel for producer-gas plants.

UP-DRAFT PLANTS.

PLANT BURNING ANTHRACITE COAL.

Plant No.	Horsepower of each gas generator.	Remarks of owner or operator regarding percentage of sulphur allowable in gas- producer fuel.					
19	300 1.5 to 1.75 per cent.						
	<u> </u>	PLANTS BURNING BITUMINOUS COAL.					
17 33 21	250 250 650, 1,000 2,500	3 per cent. 2 per cent. Not over 1 per cent. 1.5 per cent.					
		PLANT BURNING LIGNITE.					
38	300	Do not know per cent, but have seen sulphur plainly visible on fuel and had no trouble.					
		DOUBLE-ZONE PLANTS.					
		PLANTS BURNING BITUMINOUS COAL.					
2 8	250 500	1 per cent has never caused trouble; none higher used. Approximately 1.5 per cent.					

AUXILIARY POWER USED.

Many producer plants require a small amount of auxiliary power for the operation of tar extractors, blowers, pumps, exhausters, air compressors, etc. This total auxiliary power varies with the different conditions of plant operation and is, as a rule, less for plants operating with anthracite coal than for plants using tar-producing fuels. An idea of the amount of auxiliary power required may be had from the data presented in the table following, which shows the amount installed and the amount actually used.

Auxiliary power used at various producer-gas plants.

UP-DRAFT PLANTS.

	Fuel used.	Total	Total	Proportion of total plant horsepower—		
Plant No.		horsepower of plant.	horsepower of installed auxiliaries.	Installed in auxiliaries.	Actually used by auxiliaries.	
3 37 16	Lignite	300 400 400 400 500	6. 0 4. 0 18. 0 15. 0 25. 0	Per cent. 2.0 1.0 4.5 3.75 5.0	Per cent. 1.3 1.0 3.3 5.0	
26 39	Anthracite coal. do: Bituminous coal. Wood Bituminous coal.		30. 0 10. 0 15. 0 17. 0 70. 0 165. 0	6. 0 2. 0 2. 5 1. 7 6. 7 15. 0	6.0 1.3 1.7 1.9 6.2	
34 12 5	do. Anthracite coal. Bituminous coaldo.	1,500 2,500 4,000	113. 0 10. 0 65. 0 105. 0	8. 0 0. 7 2. 6 2. 6	3.9 0.7 2.6 2.0 2.8	

DOWN-DRAFT PLANTS.

200 250 500 500 1,000 3,200 6,000 9,000	5. 0 10. 0 48. 0 100. 0 170. 0 160. 0 450. 0	2.0 2.0 9.5 10.0 4.0 2.7 5.0	3.0 2.0 5.0 10.0 2.9 2.0 1.7
	250 500 500 1,000 3,200 6,000 9,000	250 5. 0 500 10. 0 500 48. 0 1,000 100. 0 3, 200 170. 0 6,000 160. 0	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$

So much depends on the details of the installation, the number of hours of service per week, and the commercial demands regarding reliability that there may be little relation between the actual auxiliary requirements of different plants. A summary of the data presented in the preceding table follows:

Summary of data regarding auxiliary power used at various producer-gas plants.

	Proportion of total plant power—						
Kind of plant.	Installed in auxiliaries.			Actually used by auxiliaries.			
	Maxi- mum.	Mini- mum.	Average.	Maxi- mum.	Mini- mum.	Average.	
Up draft Down draft	Per cent. 15. 0 10. 0	Per cent. 0.7 2.0	Per cent. 4.3 5.0	Per cent. 6. 2 10. 0	Per cent. 0.7 2.0	Per cent. 2.8 3.8	

TROUBLE FROM PRODUCER AUXILIARIES.

Data regarding serious trouble with producer auxiliaries were requested from the various owners and operators. A summary of the information furnished follows:

Data regarding trouble from auxiliaries used with gas producers.

UP-DRAFT PLANTS.

PLANTS BURNING ANTHRACITE COAL.

		PLANTS BURNING ANTHRACITE COAL.
Plant No.	Horsepower of each gas generator.	Remarks of owner or operator regarding serious trouble with producer auxiliaries,
14	75	No trouble.
6	150	Do.
9 20	160 200	Do. Do.
32	250	Do.
18	300	When fan-type exhausters were used on outlet of producer they were eaten away by sulphurous compounds.
19 36	300 300	No trouble. Do.
16	400	Do.
	·	PLANTS BURNING BITUMINOUS COAL.
3	200	No trouble.
37	200 250	Do.
33 39	370	Trouble; scrubber gets choked with tar. Tar extractors become clogged and passages of scrubbers using excessive power
00	010	cause high pressures at top of producers, causing gas to leak around poke hole, causing distress to operators. Further, under such conditions flues in fire develop rapidly when pressure is relieved at time poke holes are opened for inspection.
25	300,400	No trouble.
21 5	650, 1, 000 1, 000	Do. Do.
12	2,500	No trouble except that due to mechanical defect in steam engine driving the gas pump.
		PLANTS BURNING LIGNITE.
4	100	No trouble.
15	100 250	Do. Do.
38	300	Do.
		PLANTS BURNING WOOD.
13 26	150 250	No trouble. Do.
	'	DOWN-DRAFT PLANTS.
		PLANTS BURNING BITUMINOUS COAL.
29		No trouble.
20 27	250 250	Do. Trouble on starting new fires a little coal tar is produced, clogging exhauster.
41	200	Cleaned every 3 weeks.
35	250	No trouble.
2 8	375,500	Do.

Do. Do. Do. Do. Data regarding trouble from auxiliaries used with gas producers—Continued.

DOUBLE-ZONE PLANTS.

PLANTS BURNING BITUMINOUS COAL.

Plant No. Horsepower of each gas generator. Remarks of owner or operator regarding serious trouble with producer auxil		Remarks of owner or operator regarding serious trouble with producer auxiliaries.
2 8	250 500	No trouble. Do.
		PLANT BURNING LIGNITE.
31	200	No trouble.
		OIL-GAS PLANTS.
		PLANTS BURNING CRUDE OIL.

10	 No trouble.
30	 No trouble; wash water pump collects tar on runner shaft.

TIME REQUIRED TO BRING GAS PRODUCERS TO FULL GAS PRO-DUCTION AFTER STAND-BY.

A summary of the information furnished by owners and operators regarding the time required to bring the various types of producers to condition of normal demand after a stand-by follows:

Data regarding time required to bring various types of gas producers to condition of normal demand after a stand-by.

UP-DRAFT PLANTS.

PLANTS BURNING ANTHRACITE COAL.

Plant No.	Horsepower of each gas generator.	Remarks of owner or operator regarding time required for producer to reach full production after stand-by.
6 32 34 18 19 36	150 250 250 300 300 300 350	1 hour after 18 hours. ½ hour after 14 hours. 3 hours Monday forenoon. ½ hour after 13 hours. 1 hour after 14 hours. 40 minutes after 14 hours. ½ hour.

PLANTS BURNING BITUMINOUS COAL.

3	200 200 250 250 370 300,400 650,1,000 1,000 2,500	½ hour after 12 hours. 1 hour after 14 hours. 1 hour to come in on main line after 10 hours. 1 hour after 12 hours. 1 to 2 hours after 12 hours. 1 hour after 12 hours. 2 hour after 13 hours. 1 hour after 14 hours. 2 hour after 14 hours.
12	2,500	½ hour to 1 hour after 14 hours.

Data regarding time required to bring various types of gas producers to condition of normal demand after a stand-by—Continued.

UP-DRAFT PLANTS-Continued.

PLANTS BURNING LIGNITE.

Plant No.				
4 7 11 38	7 100 1 hour after 12 hours.			
	<u>'</u>	PLANT BURNING WOOD.		
26	200, 280	½ hour after 24 hours to 1 week.		
		DOWN-DRAFT PLANTS.		
		PLANTS BURNING BITUMINOUS COAL.		
29 27	200 250	Service continuous. Can start engine in 15 minutes after 12 hours, but takes about 1 hour to get to working well.		
23	1,500 1,500	4 hours after 32 hours. 30 minutes to 1 hour after 12 hours.		
		DOUBLE-ZONE PLANTS.		
		PLANTS BURNING BITUMINOUS COAL.		
2 8	250 500	hour after 18 hours. I hour after 16 hours.		
OIL-GAS PLANT.				

PLANT BURNING CRUDE OIL.

30	 Producer shows good efficiency after 10 minutes' operation.

STAND-BY FUEL.

Many controversies have arisen regarding the stand-by losses in producer-gas plants. What this percentage may be under test and what it is under commercial operating conditions are two widely different values. Several writers on the subject are in the habit of allowing per stand-by producer hour from 3 to 6 per cent of the fuel charged in the producer per operating hour.

An attempt was made to procure figures covering commercial operation in several plants but the returns were so greatly at variance that no deductions of value could be presented. The figures reported show stand-by percentages ranging from 3 to 33.

QUANTITY OF WATER USED BY PRODUCER PLANTS.

The quantity of water actually required in the operation of a producer-gas plant and the quantity used by the plants reporting seem to bear little relation to each other. This variance is largely due to the fact that most of the plants reporting seem to have ample water supply in close proximity so that the water cost is small.

Obviously, the quantity of water required in both the generation of the gas and in the cleaning process will vary according to the type of producer plant, the character of the fuel used, the method of operation, and the efficiency of the scrubbing devices.

QUANTITY OF VAPORIZER WATER USED.

The quantity of vapor used by the gas generators per pound of fuel fired was not reported by the operators queried. Previous investigations have indicated that for up-draft plants this figure usually runs from 0.7 to 1 pound of water for the vaporizer to each pound of anthracite coal fired. With bituminous coals, lignites, peats, wood, and other fuels the quantity of water required by the vaporizer will vary greatly with the percentage of moisture contained in the fuel. With bituminous coals in up-draft plants this figure seems to be not far from that required for anthracite coals. The average for 20 bituminous coals taken at random shows 0.7 pounds of water per pound of coal.

On the other hand, a series of investigations with one grade of fuel in an up-draft plant showed the quality of the gas to vary little for a range of vaporizer consumptions from 0.7 pound to 1.12 pounds.

In using peat it has been found that if the peat contains 25 or 30 per cent moisture no steam is necessary in the operation of the plant.

In one plant in this country operating on lignite the supply of available water is seriously limited. The moisture contained in the lignite is, however, sufficient to more than make up the vaporization requirements so that in the process of cooling the gases enough water vapor is condensed to more than offset the losses. This plant is, therefore, actually increasing its water supply during operation.

During a series of tests with a down-draft producer at the Pittsburgh station of the Bureau of Mines, the average consumption of water by the vaporizer was as follows:

Consumption of water by vaporizer in down-draft producer of Bureau of Mines.

Fuel.	Water per pound of fuel as fired, pounds.
Bituminous coal	0. 23
Lignite	
Peat	

QUANTITY OF SCRUBBER WATER USED.

The quantity of water required for scrubbing the gas in the operation of a producer-gas plant is reported by different writers as follows:

- (a) 1 gallon per 40 cubic feet of gas washed.
- (b) 3.3 gallons per brake horsepower-hour.
- (c) 10 to 15 pounds per pound of fuel used in the gas generator.

If these quantities are reduced to the basis of cubic feet of water required per 1,000 cubic feet of gas washed the range is as follows:

- (a) 3.3 cubic feet per 1,000 cubic feet of gas.
- (b) 6 cubic feet per 1,000 cubic feet of gas.
- (c) 2.6 to 3.9 cubic feet per 1,000 cubic feet of gas.

The latter figures indicate an average of approximately 4 cubic feet of water required for scrubbing 1,000 cubic feet of gas.

During the operation of the testing station of the Bureau of Mines the quantities of scrubber water averaged approximately as follows:

- $9.\overline{7}$ cubic feet per 1,000 cubic feet of gas with the up-draft plant, including the centrifugal tar extractor.
- 10.5 cubic feet per 1,000 cubic feet of gas with the down-draft plant.

Figures supplied by the operators of several plants are as follows:

Plant No.	Fuel.	Operation.	Quantity of scrubber water per pound of fuel.
37 17		Up-draftdo	
39	do		36 31 116

Quantities of scrubber water used in different gas producers.

If these figures are reduced to cubic feet of water per 1,000 cubic feet of gas washed by assuming that 1 pound of bituminous coal is equivalent to 61, 90, and 83 cubic feet of gas for up-draft, down-draft, and double-zone producers, the values are as follows:

Quantities of scrubber water used per 1,000 cubic feet of gas scrubbed.

Plant No.	Water per 1,000 cu- bic feet of gas scrubbed, cubic feet.
37	 19. 9
	6.8
39	 17. 5
25	 9.5
25	 8.1
22	 20. 6
8	 16. 9
Azzanana	14.0

The range between the temperature of the water entering and that of the water leaving the scrubber seems to depend more on the quantity of water available than on any predetermined temperature as the proper one for the water leaving the scrubber.

The prevailing temperature for the water entering the scrubber is 50° to 90° F., and for the water leaving it 75° to 200° F., the average being about 110° F.

The temperature rise recorded for the different plants is as follows:

Rise in temperature of scrubber water at different plants.

Plant No.	Temperature rise, °F.
14	45
3	8
37	10
15	50
1	155
26	37
39	44
25	45
21	
22	15
8	
2	
10	

QUANTITY OF WATER REQUIRED TO COOL ENGINE.

The quantity of water required in engine cooling is reported by various writers as follows:

- (a) For single-acting engines, 5 to 7 gallons per horsepower-hour.
- (b) For large double-acting engines, 4.5 to 5.5 gallons per horse-power-hour for cylinders, stuffing boxes, valves, etc., and 1.75 to 2.25 gallons per horsepower-hour for pistons and pistons rods; or a total ranging from 6.25 to 7.75 gallons per horsepower-hour.
- (c) Twenty-five to fifty pounds per brake horsepower-hour, or 3 to 6 gallons.
- (d) For a producer-gas engine, single-acting and of less than 200 horsepower, the normal consumption of water per brake horsepower-hour at full load is 5.5 gallons for cooling the engine.
- (e) For engines of 2 to 1,000 horsepower, for cylinder covers and stuffing boxes, 5.5 to 6.5 gallons; pistons and rods, 2 to 2.5 gallons; boxes, seats, and exhaust valves, 1 to 1.75 gallons. Total, 9 to 11 gallons per brake horsepower-hour.
- (f) With a temperature range of 90° F., 45 pounds or 5.5 gallons will be required per horsepower-hour. In large engines the consumption is smaller, or about 4.25 gallons. To be on the safe side the cooling water may be estimated at 5.5 to 8 gallons.

If the various values be reduced to the common basis of cubic feet of water per horsepower-hour, the figures are as follows:

Quantity of engine-cooling water required in various plants on basis of cubic feet per horsepower-hour.

Report.	Cooling water per horsepower-hour, cubic feet.
a	0.67 to 0.93
b	83 to 1.03
c	40 to .80
d	73 to .73
e	1.20 to 1.47
<i>f</i>	67 to 1.07
Average	75 to 1.00

The Bureau of Mines figures show an average of 0.82 cubic foot per horsepower-hour for a three-cylinder, single-acting engine of 250 horsepower.

The wide variation in practice is shown by the following figures from plant operators:

Quantity of engine-cooling water required at different producer-gas plants.

Plant No.	Cooling water per horsepower-hour, cubic feet.
37	3. 36
25	
35	2.56
22	1. 01
8	2.18
8	2. 56

The inlet temperatures reported for the cooling water range from 50° to 90° F. and the outlet temperatures from 86° to 160° F., the average being about 115° F.

LUBRICANTS USED.

The quantity of oil required per horsepower-hour varies with the character of the installation and the method of operation. For full load, 24-hour service, the proportion per horsepower-hour is of course greater than for a plant running under light load for a 9-hour or 10-hour day. Some of the figures given by the engine manufacturers for the quantity of engine oil required are as follows:

- 1. For a 200-horsepower engine, the oil amounts to 1.25 gallons per 10-hour day, or 0.625 gallon per 1,000 horsepower-hours.
- 2. For a 65-horsepower engine, the oil used is $\frac{1}{2000}$ gallon per brake horsepower-hour, or 0.500 gallon per 1,000 horsepower-hours.
- 3. For a 100-horsepower engine, inclosed crank case, 0.5 gallon per 10 hours, or 0.500 gallon per 1,000 horsepower-hours.

- 4. For a 140-horsepower engine, inclosed crank case, 1 gallon per 10 hours, or 0.715 gallon per 1,000 horsepower-hours.
- 5. For a 125-horsepower engine, inclosed crank case, 1 quart per 10 hours, or 0.200 gallon per 1,000 horsepower-hours.

The average of these quotations is 0.508 gallon per 1,000 horsepower-hours. The plant operators reported their commercial requirements to be as follows:

Plant No.	Horsepower of engines.	Length of service per day.	Cylinder oil used per 1,000 horse- power- hours.	Engine oil used per 1,000 horse- power- hours.	Other lubricants used per 1,000 horse- power- hours.
4	190 500 80,160,200,375 200,500 300 750 125	Hours. 8 16 24 24 12 24 24 10	Gallons. 2.0 1.8 2.8 1.25 1.5 1.5 5.5 13	1. 3 1. 0 3. 0 1. 26 4 .17 .4 1. 0	Gallons. 1. 25
23 24 2 30	500, 1, 000 300, 2, 000 115, 300, 750	10 24 24 24 24	2.7 .25 1.25	.6 5.3 .5	.7
Average			1.17	1.11	. 51

The average of a number of returns from the operators of reciprocating steam engines indicates the consumption of cylinder oil and engine oil to be approximately the same and to equal 0.13 gallon each per horsepower-hour. On this basis the oil consumption of gas engines seems to be approximately eight or nine times as much as that of reciprocating steam engines. This difference is perhaps not surprising, as the lubricating requirements of the gas engine are much more severe than those of the steam engine, but the ratio seems rather high.

PREIGNITIONS AND THEIR CAUSES.

Data supplied by owners and operators regarding preignitions and their causes follow. The numbers preceding each paragraph refer to plant numbers assigned by the author.

 $Are\ preignitions\ frequent\ and\ troublesome. — To\ what\ do\ you\ attribute\ them?$

UP-DRAFT PLANTS.

Plants burning anthracite coal.

- 1. Yes. Carbon deposits.
- 6. No.
- 9. No. Most trouble from too high compression.

- 14. No. Excessive hydrogen.
- 16. No.
- 18. No.
- 19. No.
- 20. No. Excessive hydrogen.
- 32. No.
- 34. No. Hydrogen.
- 36. No.

Plants burning bituminous coal.

- No, if good coal is used and valves are tight. Hydrogen, bad gas, and leaky valves.
- 12. No.
- 21. None.
- 25. No. Overhanging fire or hot particles of carbon from lubrication.
- 33. No.
- 37. No.
- 39. No.

Plants burning lignite.

- 4. Yes; at times. Carbon deposits, etc.
- 7. No.
- 11. Only for first hour after starting. Excessive hydrogen.
- 15. No.
- 38. Very seldom. To a hot spot or "chimney" in producer forming high hydrogen or to small particles of tar being sucked off governor valve and holding fire in cylinder. Stopped by throttling gas valve and then sweeping cylinder with air.

Plants burning wood.

26. Sticking valves from tar.

DOWN-DRAFT PLANTS.

Plants burning bituminous coal.

- 8. No.
- 20. No. Excessive hydrogen.
- 22. Yes. Dirt, incandescent points, too rich mixture.
- 23. No.
- 24. No.
- 27. Had trouble for a while, but seldom now. Holes or channels in fires.
- 28. After water gas run and when air inlet valve leaks. Too rich gas.
- 29. No. Do not have any.
- 35. No. Carbon.

DOUBLE-ZONE PLANTS.

Plants burning bituminous coal.

- 2. No.
- 8. No.

Plants burning lignite.

31. At times. Sticking valves.

OIL-GAS PLANTS.

Plants burning crude oil.

- 10. No. Very little. Small portions of lampblack carrying a spark.
- 30. No. Excess hydrogen under high compression.

CHANGING OR CLEANING IGNITERS.

The time interval for reliable use of engine igniters is of course more or less dependent on the constituents of the gas, the degree of cleanliness, the amount of sulphur, the engine construction, and the care in operation. The table following indicates the reported practice in this connection:

Data regarding changing or cleaning of igniters in gas producers.

UP-DRAFT PLANTS.

PLANTS BURNING ANTHRACITE COAL.

Plant No.	Period of operation each day.	Period before igniter is cleaned or changed.
14 19 16 6 9 1 34 18	Hours. 24 24 24 24 24 24 5-24 11½	Cleaned each month; lasts 4 years. 2 months. 3 month. 4 month. 5 months. 1 months. 1 months. Do.
	1	LANTS BURNING LIGNITE OR BITUMINOUS COAL.
4	8 11 24 10 14 24 24 10	\$ month. 2 months. \$\frac{1}{2} month. \$\frac{1}{2} month. \$\frac{1}{2} month. \$\frac{1}{2} to \frac{1}{2} month. \$\frac{1}{2} months. \$\frac{2}{2} months. \$\frac{2}{2} months. \$\frac{2}{2} months.
		DOWN-DRAFT PLANTS.
		PLANTS BURNING BITUMINOUS COAL.
29 27 35 22 8 23	24 10 10 10 24 24	Years. 1 month. 2 months. 2 months. 3 months.
		DOUBLE-ZONE PLANTS.
	:	PLANTS BURNING BITUMINOUS COAL OR LIGNITE.

1 month.

GAS PRESSURES AND DISTANCES FOR GAS DELIVERY.

It is interesting to note that in practically all of these plants the gas is delivered at a short distance from the producer. The reports from 36 plants show a range of distances of 15 to more than 3,000 feet. Twenty-four plants deliver their gas at distances not exceeding 100 feet and only 5 deliver gas to a distance exceeding 500 feet.

None of these plants carries gas at any considerable pressure. The range seems to be from a slightly less than atmospheric to $2\frac{1}{4}$ pounds higher than atmospheric. In the majority of instances the positive pressure ranges from 1 to 8 ounces.

RECOVERY OF BY-PRODUCTS FROM WASTE LIQUORS FROM SCRUBBERS, WASHERS, ETC.

To the query regarding recovery of by-products from waste liquors from scrubbers, washers, etc., the answers were all "None recovered" with the exception of four. Two operators report a special effort to procure the tar; one stated that he recovered the by-products, but gave no further information, and the fourth reported "Not yet."

COMMERCIAL USE MADE OF TAR PRODUCED.

The various owners and operators were asked what commercial use was made of the tar produced in their plants and what price was received for it. The data supplied are presented below. The numbers preceding each paragraph refer to plant numbers assigned by the author.

- 2. None.
- 3. None.
- 4. None.
- 5. None.
- 7. None.
- 9. No tar.
- 11. No market for tar from lignite.
- 12. Fired under boilers in main boiler plant. Saves 5 tons of coal per day, equal to \$10.
 - 13. Distilled for wood oil, creosote, and pitch.
 - 14. None recovered.
 - 17. Run back into producer.
 - 21. Burned under boiler to make steam for use in gas plant.
 - 23. No tar.
 - 24. Mixed with coal and burned in hand-fired boiler. Not satisfactory.
- 25. Utilized in steam-boiler plant. The tar from one of the producers returns to the producer and is gasified.
 - 26. Returned to producer by spreading on fuel.
 - 28. None.
 - 30. None.
 - 35. None.
 - 37. Burned under boiler.

- 38. One barrel per day goes to Puget Sound with scrubber water. Formerly burned with fuel oil under boilers, but caused some trouble on account of water. Will soon sell it or burn it again. Worth about \$1.10 per barrel if burned under boiler.
- 39. Originally provision was made for introducing the tar into the producer combustion zone, but the tar was too stiff to handle.

COMMERCIAL UTILIZATION OF CARBON RESIDUE FROM OIL-GAS PRODUCERS.

Only two replies were received to the query, Is the carbon residue from oil-gas producers commercially utilized, and if so, how? Plant 10 reported that the residue was used under boilers, and plant 30 reported that it was used as fuel in blast furnaces.

ENRICHMENT OF PRODUCER GAS.

The various owners and operators were asked whether they knew of any plants that enriched the producer gas. Replies to this inquiry indicated that the enriched producer gas was used to some degree, but not generally. Three or four companies were reported to be using this enriched gas for illuminating purposes. One plant enriched the producer gas with gasoline vapor for use in brazing.

TEMPERATURE REQUIRED AT FURNACE.

Data received from the various owners and operators regarding the temperature required at the furnace follow.

- 10. About 1,400° F.
- 12. 950 to 1,050° F. in leers.
- 13. 650° F.
- 17. 1,700° F.
- 21. 1,300 to 2,200° F.
- 24. As high as 1,500° F.
- 25. 1,500 to 2,000° F.

SPARE CAPACITY AND POWER ACTUALLY AVAILABLE.

Practically the same general rules that govern the installation of spare boiler units in steam plants control the installation of spare producer units. The principal points that have to be considered are reliability of plant and continuity of service.

The need of reserve boiler units is, however, much greater under normal operating conditions on account of the necessity of frequent boiler cleaning. Although the intermittent type of producer must be cleaned at regular intervals, depending in length on the percentage of ash in the fuel, the continuous type may be run for years without the fires being drawn if clinker troubles are not excessive.

An examination of the data at hand shows no relation between the daily hours of service and the installation of spare units. Of the plants from which reports were received, ranging in capacity from 100 to 9,000 horsepower, about one-third have reserve units of 20 to 50 per cent of the total installed power.

Ten years ago most gas producers for power purposes were overrated in capacity.

This overrating was the natural result of the blind use of European figures and became for a time a serious matter. Although the rating of such plants is far more conservative to-day, still an examination of the operating reports of 27 plants reveals the fact that approximately one-third of them have considerably less than 100 per cent of their capacity available. One instance is reported in which only 60 per cent of the rated capacity could be realized. The average percentage of available capacity for the plants that are below rating is 75.

On the other hand, 6 of the 27 plants show a capacity considerably above normal rating. The maximum is 155 per cent, and the average for the 6 is 132 per cent.

USES OF PRODUCER-GAS PLANTS.

To indicate the varied applications of producer gas and producer-gas power a brief tabulation is presented giving the information received from the 39 companies that reported. The numbers preceding the paragraphs refer to plant numbers.

- 1. Lights and power (5 to 24 hours per day).
- 2. Commercial lighting and power (24 hours per day).
- 3. Manufacture of acid phosphate (24 hours per day).
- 4. City water company (8 hours per day).
- 5. General factory purposes; also drying molds and covers.
- 6. Light and power (24 hours per day).
- 7. Milling flour (11 hours per day).
- 8. Induction motor drive (24 hours per day).
- 9. Lighting and power (24 hours per day).
- 10. Street and house lighting, ice making, refrigeration, etc. (16 hours per day).
- 11. Grinding cottonseed cake into meal for export.
- 12. Motor drives (24 hours per day, 6½ days per week). Gas also used for leers in glass bottling factory.
 - 13. For heating wood-distillation retorts (22 to 24 hours per day).
- 14. For operating blowing engines and for oprating pyrites furnace (24 hours per day.
 - 15. Light and power (14 hours per day).
 - 16. Mining and concentrating iron ore (24 hours per day).
 - 17. Hardening and annealing.
 - 18. Machine shop, electric power (11½ hours per day).
- 19. Factory lighting and power, motor-driven ammonia compressor for raw-water ice making (summer, 24 hours per day; winter, 8 to 16 hours).
 - 20. Electric lighting and power (24 hours per day).
- 21. Driving machinery by rope transmission from engine to line shaft (10 hours per day); also forge, annealing, and hardening.
 - 22. Manufacturing (10 hours per day).

- 3. Manufacture of plate glass, power (24 hours per day, 5½ days per week).
- 24. Excitation of direct-current electric generator, lights and general plant auxiliary; alternating-current motors driving grinding and polishing machines, 1,000 to 1,200 kilowatts on each alternating-current machine. (Continuous, 24 hours per day, 156 hours per week.) Also melting glass in furnaces and glass annealing.
- 25. Power in manufacturing plant (10 hours per day). Also hardening and annealing.
- 26. Power by direct drive and also direct-connected to direct-current generators (7 months, 24 hours per day; 5 months part load, 24 hours per day). Exhaust gas used to produce steam at 60 pounds pressure on vaporizers connected to engine exhausts.
 - 27. Factory power.
- 28. Electric power for phosphate mining. Principal load is motor-driven centrifugal pumps (156 hours per week).
 - 29. Oil mill, electric power (24 hours per day).
 - 30. Pumping (24 hours per day).
 - 31. Electric power (24 hours per day) and concentration of acid.
 - 32. Machine-shop power (10 hours per day) and drying linings in foundry ladles.
 - 33. Electric shop drive (14 hours).
- 34. Power in paper mill to drive beaters and pumps; also belted generators (24 hours per day, 6 days per week).
- 35. Power for manufacturing purposes, shops (10 hours per day); also for heating carbonizing furnaces.
 - 36. Power for manufacturing (10 hours per day).
 - 37. Shop power and lighting (9 hours per day).
- 38. Driving ammonia compressor and electric generator for power and light (45 months, 24 hours per day with not to exceed one stop per 20 to 30 days for cleaning and adjustments in the summer months; 7 to 8 months, 10 to 20 hours per day). Producer has had fires drawn not to exceed five times in five years.
- 39. Operating motor-driven centrifugal pumps, rotating and shaking screens and elevators, and for lighting purposes. Also conveyors, rotating dry kilns, washers, shops, etc. (24 hours per day).

RESPONSE OF PRODUCER TO SUDDEN CHANGES IN DEMAND.

Following are tabulated data relative to the response of various types of gas producers to sudden changes in demand:

Data regarding response of various types of gas producers to sudden changes in demand.

UP-DRAFT PLANTS.

PLANTS BURNING ANTHRACITE COAL.

Horsepower Reply of owner or operator to the query, "Does the gas producer respond readily to sudden changes in demand?" Plant of each gas generator. No. 350 Yes. 6..... 150 Yes; for engine load fluctuation. Starting a second engine takes about 20 minutes before gas is strong. Reasonably so. 160 Load is nearly constant. Believe it would be slow. Yes. Do. 75 400 16..... 18..... 300 19..... 300 20..... 200 32..... 250 Producer is so large that it instantly covers requirements. One alone does not. Good on full number.

 $\begin{tabular}{ll} Data\ regarding\ response\ of\ various\ types\ of\ gas\ producers\ to\ sudden\ changes\ in\ demand-\\ Continued. \end{tabular}$

UP-DRAFT PLANTS-Continued.

PLANTS BURNING BITUMINOUS COAL.

Plant No.	Horsepower of each gas generator.	Reply of owner or operator to the query, "Does the gas producer respond readily to sudden changes in demand?"
3	200 1,000 2,500 250 650, 1,000 300, 400 250 200 370	Yes; if fuel bed is in good shape. Yes. Do. Do. No trouble. Yes. No. Yes; as long as fires are kept regular. No.
		PLANTS BURNING LIGNITE.
4 7 11 15 38	100 100 250 100 300	Yes; when working well. Yes. Do. Do. Do.
		PLANTS BURNING WOOD.
13 26	150 200, 280	Yes; about 5 minutes required for increase in volume. Yes.
		DOWN-DRAFT PLANTS.
		PLANTS BURNING BITUMINOUS COAL.
8 20 22 23 24 27 28 29 35	800 250 500 1,500 1,500 250 375,500 200 250	Perfectly. Yes. Have none. Yes. Do. No. Proper care required. No. Demand is steady.

DOUBLE-ZONE PLANTS.

PLANTS BURNING BITUMINOUS COAL.

2 8	250 500	Yes. Perfectly.	
			PLANT BURNING LIGNITE.
31	200	Yes.	

PERIOD OF CONTINUOUS OPERATION.

The data following were furnished in answer to a query regarding the period of operation of gas producers.

Period of continuous operation of gas producers.

UP-DRAFT PLANTS.

PLANTS BURNING ANTHRACITE COAL.

Plant No.	Horse- power of each gas generator.	Length of service each day.	Time in continuous operation.
14	75 150 250 250 300 300 350 400	Hours. 24 24 3 to 7 24 24 10 5 to 24 24	Days. 20 Continuous Do. Do. Continuous 330
PLANTS BURNING BITUMINO	JS COAL.		
17	250 250 300 400 370 650 1,000 1,000 2,500	} 14 } 10 24 } 10 16 24	Continuous Continuous 180 to 360
PLANTS BURNING LIGHT	ITE.		
4	100 100 100 250 300	8 11 14 24 24	200 to 300 Continuous Do.
PLANTS BURNING WOO	D.		
26	150 200 280	} 24	
DOWN-DRAFT PLANTS		<u>'</u>	L
PLANTS BURNING BITUMINO	US COAL.	1	
29 20 20 27 35 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	200 250 250 250 250 375 500 500 1,500 1,500	24 24 10 10 24 10 24 24 24 24	Continuous. 30 6 6 14 10 to 15 15 to 20
DOUBLE-ZONE PLANTS	s.		
PLANT BURNING BITUMINOU	S COAL.		
2	250	24	Continuous
PLANT BURNING LIGHT	TE.		

RELIABILITY AND LENGTH OF SERVICE OF PLANTS.

The following queries were included in the general request for information sent to owners and operators of gas producers: Has the plant proved reliable? If not, what is the cause of failure? How many years has the plant been in service? The data supplied follow.

Data regarding reliability and length of service of producer-gas plants.

UP-DRAFT PLANTS.
PLANTS RURNING ANTHRACITE COAL

Plant No. Horsepower of each gas generator. Total horsepower of each gas generator. Plant.	
19	
150	
32. 250 500 Yes. In service 8 years. Reasonably so. Have had a few minor troubles, but nothing so In service 7 years. No. Too many little things that may happen to cause a shut such as change of quality of gas and poor ignition. In servyears. Yes, after some minor changes. Yes. In service 4 years. PLANTS BURNING BITUMINOUS COAL. 3. 200 400 Yes, very reliable. Plant competes with a hydroelectric plan offers current at less than 2 cents per kilowatt-hour. A part plant is run with motors, but a majority of it is run from a mas shaft. The manufacturing processes require steady power 24 haday, 7 days a week. In service 9 years. Yes. No. Tar and gas stick valves of engine and choke scrubber and No. Irregularity in thermal quality of gas. Choking of gas main engine regulators with tar. Engines are undoubtedly rated too lumproved mixing valves and gas-inlet passages would probably in increased capacity. However, considerable expense would volved. Plant has been superseded by 1,000-kilowatt steam to installed in 1911. In service 2 years. 25. 300,400 1,400 3,650 3,500 3,500 4,00	
9	
1	serious.
20. 200 Yes, after some minor changes. Yes. In service 4 years. PLANTS BURNING BITUMINOUS COAL. 3. 200 400 Yes, very reliable. Plant competes with a hydroelectric plan offers current at less than 2 cents per kilowatt-hour. A part plant is run with motors, but a majority of it is run from a mashaft. The manufacturing processes require steady power 24 h day, 7 days a week. In service 9 years. Yes. 33. 250 No. Tar and gas stick valves of engine and choke scrubber and No. Irregularity in thermal quality of gas. Choking of gas main engine regulators with tar. Engines are undoubtedly rated to Improved mixing valves and gas-inlet passages would probably in increased capacity. However, considerable expense would volved. Plant has been superseded by 1,000-kilowatt steam to installed in 1911. In service 3 years, 25. 300,400 1,400 Yes. One unit in service 3 years, and one unit 2 years. Yes. Power units in service 3 years, and one unit 2 years. Yes. Power units in service 3 years, and one unit 2 years. Yes. Power units in service 3 years; fuel unit, 1 year. After first year. At first had some trouble on account of tar and the washing equipment. Since October, 1913, have been natural gas. In service 4 years. Producers were operated 3 years continuously and were discont but are still in good condition. PLANTS BURNING LIGNITE. 4. 100 100 Producer was bought for 100 horsepower, but at present does no capacity of 90. Yes. In service 5 years. No. Unit has not been run during the past 12 months. Failure the tobe due to prejudice on the part of engineer and helpers, or pe the attention required was too tedious compared with the steam	tdown, rvice 31
PLANTS BURNING BITUMINOUS COAL. 3. 200 400 Yes, very reliable. Plant competes with a hydroelectric plan offers current at less than 2 cents per kilowatt-hour. A part plant is run with motors, but a majority of it is run from a ma shaft. The manufacturing processes require steady power 24 h day, 7 days a week. In service 9 years. 725 50 500 Yes. 730 1,100 No. Tar and gas stick valves of engine and choke scrubber and No. Irregularity in thermal quality of gas. Choking of gas mai engine regulators with tar. Engines are undoubtedly rated too Improved mixing valves and gas milet passages would probably in increased capacity. However, considerable expense would volved. Plant has been superseded by 1,000-kilowatt steam t installed in 1911. In service 2 years. 7 200,300,2,500 3,500 4,500 3,650 After first year. At first had some trouble on account of tar and the washing equipment. Since October, 1913, have been natural gas. In service 4 years. Producers were operated 3 years continuously and were discont but are still in good condition. PLANTS BURNING LIGNITE. 4 100 100 Producer was bought for 100 horsepower, but at present does no capacity of 90. Yes. In service 5 years. No. Unithas not been run during the past 12 months. Failure fit to be due to prejudice on the part of engineer and helpers, or pot the attention required was too tedious compared with the steam	
3	
offers current at less than 2 cents per kilowatt-hour. A part plant is run with motors, but a majority of it is run from a mashaft. The manufacturing processes require steady power 24 to day, 7 days a week. In service 9 years. 17. 250 500 No. Tar and gas stick valves of engine and choke scrubber and No. Irregularity in thermal quality of gas. Choking of gas main engine regulators with tar. Engines are undoubtedly rated to Improved mixing valves and gas-inlet passages would probably in increased capacity. However, considerable expense would volved. Plant has been superseded by 1,000-kilowatt steam to installed in 1911. In service 3 years, and one unit 2 years. 12. 200,300,2,500 3,500 Yes. One unit in service 3 years, fuel unit, 1 year. 25. 300,400 1,400 3,650 After first year. After shad some trouble on account of tar and the washing equipment. Since October, 1913, have been natural gas. In service 4 years. 26. 1,000 4,000 Producer were operated 3 years continuously and were discont but are still in good condition. 27. 100 Producer was bought for 100 horsepower, but at present does no capacity of 90. Yes. In service 5 years. No. Unit has not been run during the past 12 months. Failure the tobe due to prejudice on the part of engineer and helpers, or pother attention required was too tedious compared with the steam	
17. 250 500 Yes. No. Tar and gas stick valves of engine and choke scrubber and 32. 250	t of the ain line
33. 250	
engine regulators with tar. Engines are undothedry rated too Improved mixing valves and gas-inlet passages would probably in increased capacity. However, considerable expense would volved. Plant has been superseded by 1,000-kilowatt steam t installed in 1911. In service 2 years. Yes. One unit in service 3 years, and one unit 2 years. Yes. Power units in service 3 years, and one unit 2 years. Yes. Power units in service 3 years, fuel unit, 1 year. After first year. At first had some trouble on account of tar an the washing equipment. Since October, 1913, have been natural gas. In service 4 years. Producers were operated 3 years continuously and were discont but are still in good condition. PLANTS BURNING LIGNITE. Producer was bought for 100 horsepower, but at present does no capacity of 90. Yes. In service 5 years. No. Unithas not been run during the past 12 months. Failure the tob edue to prejudice on the part of engineer and helpers, or po the attention required was too tedious compared with the steam	l pipes.
25. 300, 400 1,400 Yes. One unit in service 3 years, and one unit 2 years. 21. 200,300,2,500 3,500 Yes. Power units in service 3 years, fuel unit, 1 year. 21. 650,1,000 3,650 Yes. Power units in service 3 years; fuel unit, 1 year. 22. 1,000 4,900 After first year. At first had some trouble on account of tar and the washing equipment. Since October, 1913, have been natural gas. In service 4 years. 25. 1,000 4,900 Producers were operated 3 years continuously and were discont but are still in good condition. 26. PLANTS BURNING LIGNITE. 27. 100 Producer was bought for 100 horsepower, but at present does no capacity of 90. 28. In service 5 years. 29. Yes. In service 5 years. 39. Ves. In service 5 years. 39. Ves. In service 5 years. 39. Unit has not been run during the past 12 months. Failure to be due to prejudice on the part of engineer and helpers, or pethe attention required was too tedious compared with the steam	y result d be in-
21 650,1,000 3,650 After first year. At first had some trouble on account of tar and the washing equipment. Since October, 1913, have been natural gas. In service 4 years. Producers were operated 3 years continuously and were discont but are still in good condition. PLANTS BURNING LIGNITE. Producer was bought for 100 horsepower, but at present does no capacity of 90. Yes. In service 5 years. No. Unithas not been run during the past 12 months. Failure to be due to prejudice on the part of engineer and helpers, or pot the attention required was too tedious compared with the steam	
the washing equipment. Since October, 1913, have been natural gas. In service 4 years. 1,000 4,000 Producers were operated 3 years continuously and were discont but are still in good condition. PLANTS BURNING LIGNITE. 100 Producer was bought for 100 horsepower, but at present does no capacity of 90. Yes. In service 5 years. No. Unit has not been run during the past 12 months. Failure that to be due to prejudice on the part of engineer and helpers, or pothe attention required was too tedious compared with the steam	
5 1,000 4,000 Producers were operated 3 years continuously and were discont but are still in good condition. PLANTS BURNING LIGNITE. 4 100 Producer was bought for 100 horsepower, but at present does no capacity of 90. Yes. In service 5 years. No. Unit has not been run during the past 12 months. Failure the tobe due to prejudice on the part of engineer and helpers, or pothe attention required was too tedious compared with the steam	
4	tinued,
7 100 capacity of 90. Yes. In service 5 years. No. Unit has not been run during the past 12 months. Failure the to be due to prejudice on the part of engineer and helpers, or potheattention required was too tedious compared with the steam	
 7	ot have
15 100 100 No. Unit has not been run during the past 12 months. Failure it to be due to prejudice on the part of engineer and helpers, or pot the attention required was too tedious compared with the steam	
38 300 Vos Most trouble and expense has been sittle stated	ossibly
38 300 Yes. Most trouble and expense has been with exhaust piping, trouble was overcome by installing two short sections of water-jae exhaust pipes connecting into fire-brick lined steel shell place tween the twin engines and containing a stack of cast-fron heating spiders, or star-shaped sections, which heat all jacket from 130° to 200° F. About one-half of this hot water is us industrial purposes and the balance for humidifying the prash-pit air. In service 5 years and 4 months. 11 250 500 Yes. In service 5 years.	acketed acketed aced be- a water- et water ased for

Data regarding reliability and length of service of producer-gas plants—Continued.

UP-DRAFT PLANTS-Continued.

PLANTS BURNING WOOD.

Plant No.	Horsepower of each gas generator.	Total horse- power of plant.	Reply of owner or operator to queries.
13	150	150	Yes. After finding out how to use wet wood. When plant was first started used up a large quantity of good dry wood on hand. Plant then put on very green wet wood, requiring much reconstruction of method of operation. In service intermittently for 2 years.
26	200, 280	1,040	method of operation. In service intermittently for 2 years. Yes.

DOWN-DRAFT PLANTS.

PLANTS BURNING BITUMINOUS COAL.

29	200	200	"All my figures have been destroyed, as we gave up the engine 2 years ago and have since had a fire. We are using hydroelectric power altogether and find it much more successful."
20	250		Yes, after some minor changes.
$\frac{1}{2}$	500	500	Yes. In service 71 years.
35	250	1,000	Yes. Company is now changing over to hydroelectric power. Pro-
			ducers and engines have been in service over 10 years and for many reasons are not using power economically, owing largely to rapid plant growth and necessarily poor power-plant location.
28	375,500	1,750	One pair of producers in service 6 years and one pair 2 years.
8 23	800	3,200	Yes. In service 6 years.
23	1,500	6,000	Yes. In service 4 years.
24	1,500	9,000	To certain extent. Lack of knowledge of requirements to make good quality gas, including proper grade and kind of coals, grates, steam and air supply, and method of firing and cost of apparatus.

DOUBLE-ZONE PLANT.

PLANT BURNING BITUMINOUS CCAL.

2	250	250	Fairly.	Most trouble from poor grade of coal.	In service 2½ years.

PUBLICATIONS ON FUEL TECHNOLOGY.

A limited supply of the following publications of the Bureau of Mines is temporarily available for free distribution. Requests for all publications can not be granted, and applicants should limit their selection to publications that may be of especial interest to them. Requests for publications should be addressed to the Director, Bureau of Mines, Washington, D. C.

BULLETIN 2. North Dakota lignite as a fuel for power-plant boilers, by D. T. Randall and Henry Kreisinger. 1910. 42 pp., 1 pl., 7 figs.

Bulletin 4. Features of producer-gas power-plant development in Europe, by R. H. Fernald. 1910. 27 pp., 4 pls., 7 figs.

BULLETIN 5. Washing and coking tests of coal at Denver, Colo., July 1, 1908, to June 30, 1909, by A. W. Belden, G. R. Delamater, J. J. Groves, and K. M. Way. 1910. 62 pp., 1 fig.

BULLETIN 6. Coals available for the manufacture of illuminating gas, by A. H. White and Perry Barker, compiled and revised by H. M. Wilson. 1911. 77 pp., 4 pls., 12 figs.

BULLETIN 16. The uses of peat for fuel and other purposes, by C. A. Davis. 1911. 214 pp., 1 pl., 1 fig.

BULLETIN 24. Binders for coal briquets, by J. E. Mills. 56 pp., 1 fig. Reprint of United States Geological Survey Bulletin 343.

Bulletin 27. Tests of coal and briquets as fuel for house-heating boilers, by D. T. Randall. 44 pp., 3 pls., 2 figs. Reprint of United States Geological Survey Bulletin 366.

BULLETIN 28. Experimental work conducted in the chemical laboratory of the United States fuel-testing plant at St. Louis, Mo., January 1, 1905, to July 31, 1906, by N. W. Lord. 51 pp. Reprint of United States Geological Survey Bulletin 323.

Bulletin 31. Incidental problems in gas-producer tests, by R. H. Fernald, C. D. Smith, J. K. Clement, and H. A. Grine. 29 pp., 8 figs. Reprint of United States Geological Survey Bulletin 393.

Bulletin 33. Comparative tests of run-of-mine and briquetted coal on the torpedo boat *Biddle*, by W. T. Ray and Henry Kreisinger. 50 pp., 10 figs. Reprint of United States Geological Survey Bulletin 403.

BULLETIN 36. Alaskan coal problems, by W. L. Fisher. 1911. 32 pp., 1 pl.

BULLETIN 39. The smoke problem at boiler plants, a preliminary report, by D. T. Randall. 31 pp. Reprint of United States Geological Survey Bulletin 334, revised by S. B. Flagg.

Bulletin 40. The smokeless combustion of coal in boiler furnaces, with a chapter on central heating plants, by D. T. Randall and H. W. Weeks. 188 pp., 40 figs. Reprint of United States Geological Survey Bulletin 373, revised by Henry Kreisinger.

Bulletin 49. City smoke ordinances and smoke abatement, by S. B. Flagg. 1912. 55 pp.

Bulletin 55. The commercial trend of the producer-gas power plant in the United States, by R. H. Fernald. 1913. 93 pp., 1 pl., 4 figs.

Bulletin 56. First series of gold-dust tests in the experimental mine, by G. S. Rice, L. M. Jones, J. K. Clement, and W. L. Egy. 1913. 115 pp., 12 pls., 28 figs.

Bulletin 58. Fuel-briquetting investigations, July, 1904, to July, 1912, by C. L. Wright. 1913. 277 pp., 21 pls., 3 figs.

Bulletin 76. United States coals available for export trade, by Van. H. Manning. 1914. 15 pp., 1 pl.

BULLETIN 85. Analyses of mine and car samples of coal collected in the fiscal years 1911 to 1913, by A. C. Fieldner, H. I. Smith, A. H. Fay, and Samuel Sanford. 1914. 444 pp., 2 figs.

Bulletin 116. Methods of sampling delivered coal and specifications for the purchase of coal for the government, by G. S. Pope. 1916. 64 pp., 5 pls., 2 figs.

TECHNICAL PAPER 2. The escape of gas from coal, by H. C. Porter and F. K. Ovitz. 1911. 14 pp., 1 fig.

TECHNICAL PAPER 5. The constituents of coal soluble in phenol, by J. C. W. Frazer and E. J. Hoffman. 1912. 20 pp., 1 pl.

TECHNICAL PAPER 8. Methods of analyzing coal and coke, by F. M. Stanton and A. C. Fieldner. 1913. 42 pp., 12 figs.

TECHNICAL PAPER 9. The status of the gas producer and of the internal-combustion engine in the utilization of fuels, by R. H. Fernald. 1912. 42 pp., 6 figs.

TECHNICAL PAPER 10. Liquefied products of natural gas; their properties and uses, by I. C. Allen and G. A. Burrell. 1912. 23 pp.

TECHNICAL PAPER 16. Deterioration and spontaneous combustion of coal in storage, a preliminary report, by H. C. Porter and F. K. Ovitz. 1912. 14 pp.

TECHNICAL PAPER 34. Experiments with furnaces for a hand-fired return tubular boiler, by S. B. Flagg, G. C. Cook, and F. E. Woodman. 1914. 32 pp., 1 pl., 4 figs.

TECHNICAL PAPER 35. Weathering of the Pittsburgh coal bed at the experimental mine near Bruceton, Pa., by H. C. Porter and A. C. Fieldner. 1914. 35 pp., 14 figs. Technical Paper 37. Heavy oil as fuel for internal-combustion engines, by I. C.

Allen. 1913. 36 pp.

TECHNICAL PAPER 38. Wastes in the production and utilization of natural gas, and methods for their prevention, by Ralph Arnold and F. G. Clapp. 1913. 29 pp.

TECHNICAL PAPER 45. Waste of oil and gas in the Mid-Continent fields, by R. S. Blatchley. 1914. 54 pp., 2 pls., 15 figs.

TECHNICAL PAPER 49. The flash point of oils—methods and apparatus for its determination, by I. C. Allen and A. S. Crossfield. 1913. 31 pp., 2 figs.

TECHNICAL PAPER 50. Metallurgical coke, by A. W. Belden. 1913. 48 pp., 1 pl., 23 figs.

TECHNICAL PAPER 55. The production and use of brown coal in the vicinity of Cologne, Germany, by C. A. Davis. 1913. 15 pp.

TECHNICAL PAPER 57. A preliminary report on the utilization of petroleum and natural gas in Wyoming, by W. R. Calvert, with a discussion of the suitability of natural gas for making gasoline, by G. A. Burrell. 1913. 23 pp.

TECHNICAL PAPER 63. Factors governing the combustion of coal in boiler furnaces; a preliminary report, by J. K. Clement, J. C. W. Frazer, and C. E. Augustine. 1914. 46 pp., 26 figs.

TECHNICAL PAPER 64. The determination of nitrogen in coal, a comparison of various modifications of the Kjeldahl method with the Dumas method, by A. C. Fieldner and C. A. Taylor. 1915. 25 pp., 5 figs.

TECHNICAL PAPER 65. A study of the oxidation of coal, by H. C. Porter. 1914. 30 pp., 12 figs.

TECHNICAL PAPER 74. Physical and chemical properties of the petroleums of California, by I. C. Allen, W. A. Jacobs, A. S. Crossfield, and R. R. Mathews. 1914. 38 pp., 1 fig.

TECHNICAL PAPER 76. Notes on the sampling and analysis of coal, by A. C. Fieldner. 1914. 59 pp., 6 figs.

TECHNICAL PAPER 89. Coal-tar products and the possibility of increasing their manufacture in the United States, by H. C. Porter, with a chapter on coal-tar products used in explosives, by C. G. Storm. 1915. 21 pp.

TECHNICAL PAPER 97. Saving fuel in heating a house, by L. P. Breckenridge and S. B. Flagg. 1915. 35 pp., 3 figs.

TECHNICAL PAPER 104. Analysis of natural gas and illuminating gas by fractional distillation at low temperatures and pressures, by G. A. Burrell, F. M. Seibert, and I. W. Robertson. 1915. 41 pp., 7 figs.

TECHNICAL PAPER 112. The explosibility of acetylene, by G. A. Burrell and G. G. Oberfell. 1915. 15 pp.

TECHNICAL PAPER 123. Notes on the uses of low-grade fuel in Europe, by R. H. Fernald. 1915. 37 pp.

PUBLICATIONS THAT MAY BE OBTAINED ONLY THROUGH THE SUPER-INTENDENT OF DOCUMENTS.

The editions for free distribution of the following Bureau of Mines publications are exhausted, but copies may be obtained by purchase from the Superintendent of Documents, Government Printing Office, Washington, D. C., or can be consulted at public libraries. Prepayment of the price is required and should be made in cash (exact amount) or by postal or express money order payable to the Superintendent of Documents.

The Superintendent of Documents is an official of the Government Printing Office and is not connected with the Bureau of Mines.

BULLETIN 1. The volatile matter of coal, by H. C. Porter and F. K. Ovitz. 1910. 56 pp., 1 pl., 9 figs. 10 cents.

BULLETIN 3. The coke industry of the United States as related to the foundry, by Richard Moldenke. 1910. 32 pp. 5 cents.

Bulletin 7. Essential factors in the formation of producer gas, by J. K. Clement, L. H. Adams, and C. N. Haskins. 1911. 58 pp., 1 pl., 16 figs. 10 cents.

BULLETIN 9. Recent development of the producer-gas power plant in the United States, by R. H. Fernald. 1910. 82 pp., 2 pls. 15 cents. Reprint of United States Geological Survey Bulletin 416.

Bulletin 11. The purchase of coal by the Government under specifications, with analyses of coal delivered for the fiscal year 1908–9, by G. S. Pope. 80 pp. 10 cents. Reprint of United States Geological Survey Bulletin 428.

Bulletin 12. Apparatus and methods for the sampling and analysis of furnace gases, by J. C. W. Fraser and E. J. Hoffman. 1911. 22 pp., 6 figs. 5 cents.

BULLETIN 13. Resumé of producer-gas investigations, October 1, 1904, to June 30, 1910, by R. H. Fernald and C. D. Smith. 1911. 393 pp., 12 pls., 250 figs. 65 cents. BULLETIN 18. The transmission of heat into steam boilers, by Henry Kreisinger and W. T. Ray. 1912. 180 pp., 78 figs. 20 cents.

Bulletin 14. Briquetting tests of lignite at Pittsburgh, Pa., 1908–9, with a chapter on sulphate-pitch binder, by C. L. Wright. 1911. 64 pp., 11 pls., 4 figs. 15 cents. Bulletin 22. Analyses of coals in the United States, with descriptions of mine and field samples collected between July 1, 1904, and June 30, 1910, by N. W. Lord, with chapters by J. A. Holmes, F. M. Stanton, A. C. Fieldner, and Samuel Sanford. 1912. Part I, Analyses, pp. 1–321; Part II, Descriptions of samples, pp. 321–1129. 85 cents.

BULLETIN 23. Steaming tests of coals and related investigations, September 1, 1904, to December 31, 1908, by L. P. Breckenridge, Henry Kreisinger, and W. T. Ray. 1912. 380 pp., 2 pls., 94 figs. 50 cents.

BULLETIN 29. The effect of oxygen in coal, by David White. 80 pp., 3 pls. 20 cents. Reprint of United States Geological Survey Bulletin 382.

BULLETIN 30. Briquetting tests at the United States fuel-testing plant, Norfolk, Va., 1907–8, by C. L. Wright. 41 pp., 9 pls. 15 cents. Reprint of United States Geological Survey Bulletin 385.

BULLETIN 32. Commercial deductions from comparisons of gasoline and alcohol tests on internal-combustion engines, by R. M. Strong. 38 pp. 5 cents. Reprint of United States Geological Survey Bulletin 392.

BULLETIN 34. Tests of run-of-mine and briquetted coal in a locomotive boiler, by W.T. Ray and Henry Kreisinger. 33 pp., 9 figs. 5 cents. Reprint of United States Geological Survey Bulletin 412.

BULLETIN 35. The utilization of fuel in locomotive practice, by W. F. M. Goss. 29 pp., 8 figs. 5 cents. Reprint of United States Geological Survey Bulletin 402.

BULLETIN 41. Government coal purchases under specifications, with analyses for the fiscal year 1909–10, by G. S. Pope, with a chapter on the fuel-inspection laboratory of the Bureau of Mines, by J. D. Davis. 1912. 97 pp., 3 pls., 9 figs. 15 cents.

Bulletin 43. Comparative fuel values of gasoline and denatured alcohol in internal-combustion engines, by R. M. Strong and Lauson Stone. 1912. 243 pp., 3 pls., 32 figs. 20 cents.

BULLETIN 54. Foundry-cupola gases and temperature, by A. W. Belden. 1913. 29 pp., 3 pls., 16 figs. 10 cents.

Bulletin 63. Sampling coal deliveries and types of Government specifications for the purchase of coal, by G. S. Pope. 1913. 68 pp., 4 pls., 3 figs. 10 cents.

Bulletin 97. Sampling and analysis of flue gases, by Henry Kreisinger and F. K. Ovitz. 1915. 68 pp., 1 pl., 37 figs. 15 cents.

TECHNICAL PAPER 1. The sampling of coal in the mine, by J. A. Holmes. 1911. 18 pp., 1 fig. 5 cents.

TECHNICAL PAPER 3. Specifications for the purchase of fuel oil for the Government, with directions for sampling oil and natural gas, by I. C. Allen. 1911. 13 pp. 5 cents.

TECHNICAL PAPER 25. Methods for the determination of water in petroleum and its products, by I. C. Allen and W. A. Jacobs. 1912. 13 pp., 2 figs. 5 cents.

TECHNICAL PAPER 26. Methods for the determination of the sulphur content of fuels, especially petroleum products, by I. C. Allen and I. W. Robertson. 1912. 13 pp., 1 fig. 5 cents.

TECHNICAL PAPER 109. Composition of the natural gas used in 25 cities, with a discussion of the properties of natural gas, by G. A. Burrell and G. G. Oberfell. 1915. 22 pp. 5 cents.

TECHNICAL PAPER 114. Heat transmission through boiler tubes, by Henry Kreisinger and J. F. Barkley. 1915. 36 pp. 23 figs. 10 cents.

TECHNICAL PAPER 115. Inflammability of mixtures of gasoline vapor and air, by G. A. Burrell and H. T. Boyd. 1915. 18 pp., 2 figs. 5 cents.

INDEX.

A. Page.	E. Page.
•	,
Analyses, of Big Muddy, Ill., run-of-mine coal 17, 19	Eccentric revolving-grate producers. See Gas
of bituminous coal	producers.
of buckwheat coal14	Engine, cooling of, water for 55-56
of Hocking Valley coal	lubricating of, cost of
of Illinois bituminous coal	oil for 56-57
of lignite	Europe, gas producers in, demand for 7
of New River coal	producer-gas plants in, fuel capacity of 8
	slagging gas producers in 9
of pea anthracite	_
of Pennsylvania coals	F.
of Pocahontas slack	Fires in gas producers, periods of drawing 39
of producer gas	Fuel, conservation of, need for 9,12
of Texas lignite	for gas producers, character of 14-19
of West Virginia bituminous coal 18	grades of 9,11–14
Anthracite coal, advantages of, for gas pro-	sizes of
ducers	from refuse heaps, utilization of
	heating value of, per pound as fired 12
consumption of, per brake horsepower-	high-ash, use of
hour	Fuel bed, area of, fuel consumption relative to 20-23
relation of, to fuel-bed area 20–21, 24	relation of, to pokings
operation of gas producers with, cost of 14	depth of, relation of, to fuel consumption. 27-28
pea, analyses of	
Ash, in gas-producer fuel, percentage of 12, 13	
Auxiliaries, for producer-gas plants, horse-	notes and characters are, the above the
power of	F 8 - 7
trouble with 50-51	Fuel charges, time between, relation of, to
tiouble with	weight 32
В.	Fuel consumption, in gas producers, conclu-
	sions regarding
Big Muddy, Ill., run-of-mine coal from, analy-	rate of 19–27
ses of	per brake horsepower-hour
Bituminous coal, analyses of 15–19	per hour in gas producers
consumption of, per brake horsepower-	relation of, to fuel-bed area 20-23
hour 24, 26	to grate area
relation of, to fuel-bed area 21-24	to pokings of fuel bed
cost of operation with	See also Heating value of fuel.
use of, in gas producers	Fuel tests, results of
See also Big Muddy, Ill.; Hocking Valley;	Furnace, temperature required at
	G.
Illinois; Pennsylvania; Pocahon-	y.
tas slack; West Virginia.	Gas. See Producer gas.
Bone, tests of	Gas generators. See Producer-gas generators.
Brazil, run-of-mine coal from, tests of	Gas-producer products, cost of
Buckwheat coal. See Coal.	Gas producers, classification of 5
Burners, gas, effect of tar and lampblack on 47	condition of, after stand-by 51-52
By-products, from gas producers, recovery of .8-9, 60	demand for, in Europe 7
	down-draft, fuel used in 17-19
С.	eccentric revolving grate, advantages of 7,8
Capacity, spare, available at producer-gas	operation of, period of
	response of, to sudden changes in demand 63-64
plants	time for full production of, after stand-by. 51-52
Carbon residue, commercial use of	up-draft, fuel used in
Cleaning of gas producers. See Producer-gas	See also Producer-gas generators; Pro-
generators.	ducer-gas plants.
Clinkering in gas producers, trouble from6,7,14	Germany, gas producers in, types of
Clinkering coals, steam required for 8	Grate area, of gas producers, relation of, to fuel
Coal, buckwheat, analyses of	
low-sulphur, necessity for 14, 15, 18	consumption 27-28
See also Anthracite coal; Bituminous	н.
coal; Run-of-mine coal.	Heating value of fuel, per pound as fired 12
· · · · · · · · · · · · · · · · · · ·	and the second s
Coal consumption. See Fuel consumption.	relation of, to fuel consumption 26
Coke, use of, as by-product	Heating value of producer gas, from anthra-
Coke breeze, use of, in gas producers 9	cite coal
Coke-oven gas, production and use of 8-9	from bituminous coal

rage.	rage.
Heating value of producer gas, from lignite 30,31	Producer gas, from peat, analyses of 30
from peat 30, 31	heating value of 30–31
from wood	production of
Hocking Valley coal, analyses of	from wood, analyses of
Horsepower, of producer-gas generators 20-23,	heating value of
25, 32, 35-48, 50-53	pressures of
of producer-gas plants 25, 36-39, 49, 61-62	scrubbing and cleaning of 40-43
_	variations in, overcoming of
I.	Producer-gas generators, cleaning of 36-38
Igniters, engine, changing and cleaning of 59	horsepower of 20-23, 25, 32, 35-48, 50-53
See also Preignitions.	Producer-gas plants, capacity and power
Illinois, bituminous coal from, analyses of 18	available at
bone from, tests of	commercial, comparison of, with Govern-
Iowa, coal from, tests of	ment station
T	horsepower of
L.	number of, in United States
Labor cost, reduction of	reliability and service of
Lampblack, effect of, on cost of engine lubri-	stand-by losses in
cation	water used in 53–56
in gas producers, trouble from 45, 47	See also Gas producers.
Lignite, analyses of	
consumption of, per brake horsepower-	Producer-gas power, applications of 62-63
hour 24, 26	R.
relation of, to fuel-bed area 22-24	70 4 11 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
use of, in producer-gas plants 5,6	Run-of-mine coal, tests of
water in, percentage of	_
Lignite screenings, analyses of	S.
use of, as fuel in gas producers	Scrubber material, renewals of, time between. 41-42
Lubrication of engine, cost of, effect of tar or	Scrubbing of gas. See Producer gas.
lampblack on	Slagging gas producer, use of, in Europe 9
Lubricants, for engine, quantity of	Stand-by. See Gas producers.
	Steam turbine, installation of, in producer-gas
М.	
Moisture, in gas-producer fuel, percentage of . 13	plants 10-11 Steel manufacture of cost of 13
Moisture, in gas-producer fuel, percentage of . 13 See also Water.	Steel, manufacture of, cost of
See also Water.	Steel, manufacture of, cost of
See also Water. N.	Steel, manufacture of, cost of
See also Water. N. New Mexico, run-of-mine coal from, tests of 13	Steel, manufacture of, cost of
See also Water. N.	Steel, manufacture of, cost of
See also Water. N. New Mexico, run-of-mine coal from, tests of	Steel, manufacture of, cost of
See also Water. N. New Mexico, run-of-mine coal from, tests of	Steel, manufacture of, cost of
N. New Mexico, run-of-mine coal from, tests of 13	Steel, manufacture of, cost of
N. New Mexico, run-of-mine coal from, tests of . 13	Steel, manufacture of, cost of
N. New Mexico, run-of-mine coal from, tests of . 13	Steel, manufacture of, cost of
N. New Mexico, run-of-mine coal from, tests of . 13	Steel, manufacture of, cost of
N. New Mexico, run-of-mine coal from, tests of 13 New River coal, analyses of 16 P. Peat, consumption of, per brake horsepower-hour 24, 26 relation of, to fuel-bed area 24 use of, in production of sulphate of ammonia 8	Steel, manufacture of, cost of
N. New Mexico, run-of-mine coal from, tests of 13 New River coal, analyses of 16 P. Peat, consumption of, per brake horsepower-hour 24, 26 relation of, to fuel-bed area 24 use of, in production of sulphate of ammonia 8 Pennsylvania, coal from, analyses of 18	Steel, manufacture of, cost of
N. New Mexico, run-of-mine coal from, tests of . 13 New River coal, analyses of . 16 P. Peat, consumption of, per brake horsepower-hour . 24, 26 relation of, to fuel-bed area . 24 use of, in production of sulphate of ammonia . 8 Pennsylvania, coal from, analyses of . 18 washery refuse from, tests of . 13	Steel, manufacture of, cost of
N. New Mexico, run-of-mine coal from, tests of . 13 New River coal, analyses of . 16 P. Peat, consumption of, per brake horsepower-hour. 24, 26 relation of, to fuel-bed area 24 use of, in production of sulphate of ammonia 8 Pennsylvania, coal from, analyses of 18 washery refuse from, tests of 13 Pitch, from gas producers, recovery of 9	Steel, manufacture of, cost of
N. New Mexico, run-of-mine coal from, tests of. 13	Steel, manufacture of, cost of
N. New Mexico, run-of-mine coal from, tests of 13 New River coal, analyses of 16 P. Peat, consumption of, per brake horsepower-hour 24, 26 relation of, to fuel-bed area 24 use of, in production of sulphate of ammonia 8 Pennsylvania, coal from, analyses of 13 Pitch, from gas producers, recovery of 9 Pocahontas slack, analyses of 15 Pokings of fuel bed . See Fuel bed	Steel, manufacture of, cost of
New Mexico, run-of-mine coal from, tests of 13	Steel, manufacture of, cost of
N. New Mexico, run-of-mine coal from, tests of . 13 New River coal, analyses of . 16 P. Peat, consumption of, per brake horsepower-hour . 24, 26 relation of, to fuel-bed area . 24 use of, in production of sulphate of ammonia . 8 Pennsylvania, coal from, analyses of . 18 washery refuse from, tests of . 13 Pitch, from gas producers, recovery of . 9 Pocahontas slack, analyses of . 15 Pokings of fuel bed . See Fuel bed . Power, rating of, at producer-gas plants . 61-62 See also Horsepower; Producer-gas power .	Steel, manufacture of, cost of
New Mexico, run-of-mine coal from, tests of 13	Steel, manufacture of, cost of
New Mexico, run-of-mine coal from, tests of 13	Steel, manufacture of, cost of
New Mexico, run-of-mine coal from, tests of 13	Steel, manufacture of, cost of
New Mexico, run-of-mine coal from, tests of 13 New River coal, analyses of 16 P. Peat, consumption of, per brake horsepower-hour 24, 26 relation of, to fuel-bed area 24 use of, in production of sulphate of ammonia 8 Pennsylvania, coal from, analyses of 18 washery refuse from, tests of 13 Pitch, from gas producers, recovery of 9 Pocahontas slack, analyses of 15 Pokings of fuel bed See Fuel bed 15 Power, rating of, at producer-gas plants 61-62 See also Horsepower; Producer-gas power 16 Predignitions, causes of 57-59 Producer gas, analyses of 28-30 applications of 62-63 delivery of 60	Steel, manufacture of, cost of
New Mexico, run-of-mine coal from, tests of 13 New River coal, analyses of 16 P. Peat, consumption of, per brake horsepower-hour 24, 26 relation of, to fuel-bed area 24 use of, in production of sulphate of ammonia 8 Pennsylvania, coal from, analyses of 18 washery refuse from, tests of 13 Pitch, from gas producers, recovery of 9 Pocahontas slack, analyses of 15 Pokings of fuel bed See Fuel bed 15 Power, rating of, at producer-gas plants 61-62 See also Horsepower; Producer-gas power 16 Predignitions, causes of 57-59 Producer gas, analyses of 28-30 applications of 62-63 delivery of 60	Steel, manufacture of, cost of
New Mexico, run-of-mine coal from, tests of 13	Steel, manufacture of, cost of
New Mexico, run-of-mine coal from, tests of 13	Steel, manufacture of, cost of
New Mexico, run-of-mine coal from, tests of 13	Steel, manufacture of, cost of
New Mexico, run-of-mine coal from, tests of 13	Steel, manufacture of, cost of
New Mexico, run-of-mine coal from, tests of 13	Steel, manufacture of, cost of.
New Mexico, run-of-mine coal from, tests of 13	Steel, manufacture of, cost of
New Mexico, run-of-mine coal from, tests of 13	Steel, manufacture of, cost of
New Mexico, run-of-mine coal from, tests of 13	Steel, manufacture of, cost of

 \cap